

Original Research Article

Optimization of Acid Activated Ngbo Clay Catalysts in Esterification Reaction Using Response Surface Methodology

ABSTRACT

In this study, Box-Behnken's Response Surface Methodology (RSM) was applied to study the esterification reaction effectiveness of acid activated Ngbo clay catalyst. The esterification were monitored based on the process conditions of temperature, duration, amount of reactant, catalyst weight and particle size. The Box--Behnken's Response Surface Methodology indicates that the acid clay-catalysed esterification reactions proceed through dual mechanisms of Acid-complex and Alcohol-complex mechanisms with the Alcohol mechanism dominating. The esterification efficiencies of acetic acid and ethanol by acid activated Ngbo clay catalyst optimized using RSM models indicated the estimated esterification percentage of >99%. The predicted and experimental values under the same conditions showed less than 5% difference thereby making the Box-Behnken design approach an efficient, effective and reliable method for the esterification of acetic acid with ethanol. The produced catalyst was optimized using A-One way ANOVA modelling, which indicated correlation coefficient of the regression of 0.9940, which implies that 99.40% of the total variation in the esterification reaction was attributed to the experimental variables. The result obtained indicated that the process could be applied in the esterification of acetic acid to avoid the drawbacks of corrosion, loss of catalyst and environmental problems.

Keywords: Optimization, Characterization, Esterification, Acid Activated Clay Catalyst, Response Surface Methodology, Box-Behnken design

1. INTRODUCTION

Esterification reactions has long been carried out in homogeneous phase in the presence of acid catalysts such as sulphuric acid, hydrochloric acid and p – toluene sulfonic acid (p – TSOH); which has drawbacks of corrosion, loss of catalyst and environmental problems [1, 2]. Therefore, researches have been focused to develop eco-friendly heterogeneous catalysts for synthesis of fatty acid esters. The most popular solid acids catalyst used to produce esters

were ion-exchange organic resins, such as Amberlyst – 15 [3, 4], Zeolites [5 – 6], [7] and Silica-supported heteropoly acid [8] and [9]. Nevertheless, they have shown limitations in applicability for catalysing esterification reaction due to low thermal stability (Amberlyst-15 < 140°C), mass transfer resistance (Zeolites) [10], [11], or loss of active acid sites in the presence of a polar medium (HPA/silica) [9].

Clay is one of the raw materials in abundance in Nigeria. It is readily available in Nigeria in large deposit yet its potentials have not been fully explored. However, there is recent interest in exploring the potentials of clays such in bleaching of palm oil [12, 13], in adsorption of dyes [14 – 16] among others. In a quest to develop green processes, clay is mostly used in the synthesis of catalysts, although use of Nigerian clays from Ngbo, Ohaukwu- Ebonyi State for producing clay catalysts is limited in literature. Though the kinetics of clay-catalysed esterification reactions is abundant in literature, but with little or no data on the mechanistic and empirical modelling on the use of Ngbo clay in this regard.

Response Surface Methodology (RSM) is a collection of statistical and mathematical techniques that uses quantitative data. Central composite design (CCD), Box-Behnken and Doehlert designs (BBD) are among the principal response surface methodologies used in experimental design. This method is suitable for fitting a quadratic surface and it helps to optimize the effective parameters with a minimum number of experiments, and also to analyze the interaction between the parameters [4]. The objective is to optimize a response (output variable) which is influenced by several independent variables (input variables). The application of RSM to design optimization is aimed at reducing the cost of expensive numerous experiments, saving time, reducing stress, etc [17 – 20].

This work investigated the use of local clay from Ngbo in Ohaukwu Local Government Area of Ebonyi State Nigeria for the production of acid activated catalyst and optimizes the effectiveness of the clay catalyst for esterification of acetic acid with ethanol using Response Surface Methodology.

2. Materials and Methods

Comment [A1]: Please specify all the materials used in this research

2.1 Source of Raw Materials

The clay sample was obtained from Ngbo in Ohaukwu L.G.A. of Ebonyi State (N 06°30' 32.8''), (E 007°58'13.7'').

2.2 Physico-Chemical Characterization of Ngbo Clay

The Ngbo clay sample was subjected to some physical analysis in order to obtain their physical properties. The analysis carried out include: Bulk density, Moisture content, pH and Loss on Ignition (LOI).

2.3 Characterisation of the raw clay and acid activated sample

The Ngbo clay sample was characterised using XRF and XRD.

2.4 Acid Activation

The acid activation method used in this work is as reported by [21]. A 100g of pulverized and screened clay was mixed into slurry with 50ml of diluted water, 30ml of 1M H₂SO₄ was added and stirred vigorously and placed in an oven where it was maintained at a temperature of 100°C. The sample was washed thereafter and left to sediment. Complete removal of all residual acid was achieved by repeating washing and decanting until a pH of six was obtained. The final slurry was filtered and dried at 100°C. The dried, activated and washed clay was then pulverized, screened and stored in desiccators prior to use.

Comment [A2]: write down the time required for activation

2.5 Optimization of Process Conditions on the Catalyst Quality Produced Using Esterification Process

2.5.1 Sample Preparation/Procedure

The raw clay sample was crushed, sieved at 100microns, 200microns and 300microns. Thereafter, the clay sample was activated using acid (H₂SO₄) method. The acid activated clay sample was used in esterification reaction to assess the effectiveness. Predetermined weight of the clay sample was weighed; one mole of Ethanol and acetic acid was each pipetted into the clay sample to ensure that the active sites of the catalyst were not blocked by the ethanol. The container was tightly closed, the contents was shaken vigorously and immersed in a water bath shaker maintained at the conditions of the experimental design in Table.1. The summary of the reaction equation is:



On titration, the equation becomes:



Table 1: The natural and coded values of the independent variables used

| VARIABLES | NATURAL VALUES | | | CODED VALUES | | |
|-------------------------------|----------------|-----------|------------|--------------|-----------|------------|
| | Low level | Mid-point | High level | Low level | Mid Point | High level |
| Temperature (°C), A | 50 | 70 | 90 | -1 | 0 | +1 |
| Process duration (minutes), B | 30 | 195 | 360 | -1 | 0 | +1 |
| Excess reactant (ml), C | 2.5 | 3.75 | 5 | -1 | 0 | +1 |
| Catalyst weight (grammes), D | 0.25 | 0.38 | 0.5 | -1 | 0 | +1 |
| Particle size (microns), E | 100 | 200 | 300 | -1 | 0 | +1 |

The clay-catalysed esterification was modelled using Box-Behnken Response Surface Methodology.

For five factors inputs of x_1 , x_2 , x_3 , x_4 and x_5 , the equation of the quadratic response is given as;

$$Y = b_0 + b_1X_1 + b_2X_2 + b_3X_3 + b_4X_4 + b_5X_5 + b_{12}X_1X_2 + b_{13}X_1X_3 + b_{14}X_1X_4 + b_{15}X_1X_5 + b_{23}X_2X_3 + b_{24}X_2X_4 + b_{25}X_2X_5 + b_{34}X_3X_4 + b_{35}X_3X_5 + b_{45}X_4X_5 + b_{11}X_1^2 + b_{22}X_2^2 + b_{33}X_3^2 + b_{44}X_4^2 + b_{55}X_5^2. \quad (3)$$

2.6 Response Surface Methodology

The response surface technique applying Box-behnken design matrix was applied to study the interaction and effects among the factors and their level of contributions and significance in the clay-catalysed esterification. This method determines the needed best working conditions in a shorter time and detailed conditions of processes are provided. This was achieved through a designed experimental design applying Box-Behnken Response Surface Methodology design of 46 steps of experiment consisting five factors and three levels.

3. RESULTS AND DISCUSSION

3.1 Physical properties of the raw clay

The result of the physical properties of raw Ngbo clay is presented in [table 2](#). The result showed that the clay has a moisture content of 3.3 % and bulk density of 1.25 g/ml, which are in agreement with the previous research of [22 – 24] that reported the moisture content of kaolinite clay is between 3.0 – 4.0% and the bulk density is 1.2 – 1.4 g/ml.

Comment [A3]: check the writing format

Table 2: Results of Bulk density, Moisture content, pH, and LOI

| Clay type | Bulk density (g/ml) | % moisture content | pH | LOI (%) |
|-----------|---------------------|--------------------|-----|---------|
| Ngbo clay | 1.25 | 3.33 | 7.5 | 10.52 |

3.2 Characterization of Raw Clay and Acid Activated Clay

The chemical properties of the raw Ngbo clay was analysed using XRF and XRD.

The result of the XRF composition analysis of raw Ngbo clay and Acid activated Ngbo clays (AAC) is presented in Table 3. The result showed that raw and activated clays have [contaminations of oxides](#) and other impurities, but the clay minerals compositions are not meaningfully affected by acid treatments even under strong conditions and below 500 °C as reported in literature by [25, 26] and [27]. This shows that improvement on the properties of the clay by chemical methods below 500 °C is difficult due to its low reactivity. This result of the XRF on the Ngbo raw clay and acid activated Ngbo clays as shown in [table 4](#) also indicates high content of silicon and [aluimium](#) oxides compared to other oxides.

Comment [A4]: oxide contaminants ?

Comment [A5]: Table 4

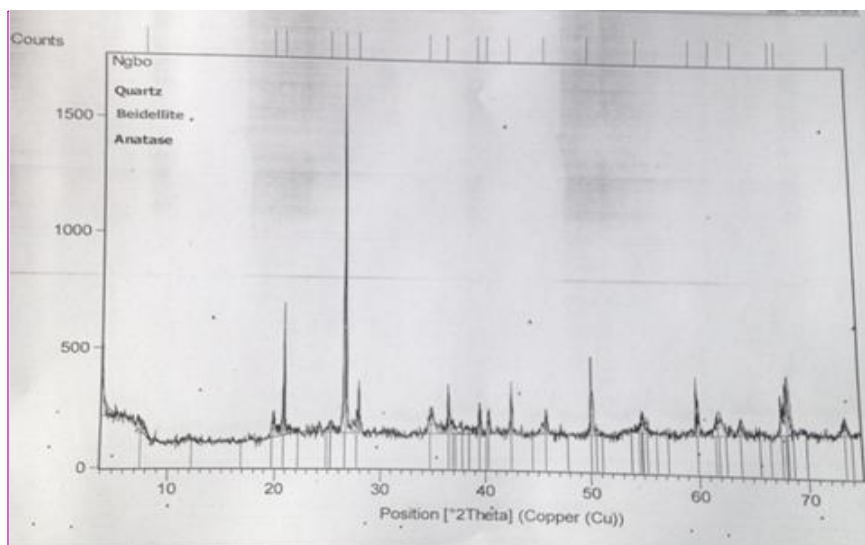
Table 3: Results of XRF analysis of raw Ngbo Clay and acid activated Ngbo clay

| Chemical constituent | Raw clay (Wt. %) | Acid activated (AAC), (Wt. %) |
|--------------------------------|------------------|-------------------------------|
| SiO ₂ | 62.70 | 67.030 |
| TiO ₂ | 1.52 | 1.285 |
| Al ₂ O ₃ | 19.70 | 23.924 |
| Fe ₂ O ₃ | 2.06 | 4.968 |
| P ₂ O ₃ | – | 0.149 |
| CaO | 0.789 | 0.143 |

| | | |
|--------------------------------|-------|-------|
| MgO | 0.026 | 0.646 |
| Na ₂ O | 0.20 | 0.057 |
| K ₂ O | 0.85 | 1.109 |
| Mn ₂ O ₃ | – | 0.079 |
| V ₂ O ₅ | 0.071 | – |
| Cr ₂ O ₃ | 0.035 | 0.012 |
| CuO | 0.044 | – |
| BaO | 0.19 | – |
| L.O.I | 11.82 | – |
| SO ₃ | – | 0.573 |
| Cl | – | 0.008 |
| ZnO | – | 0.013 |
| SrO | – | 0.006 |

The results of XRD pattern analysis of raw Ngbo clay is presented in [figure 1](#). The results of XRD pattern results showed several characteristic peaks due to minerals compositions present. The peak obtained at position corresponding to $2\theta = 22.64^\circ$ indicated the presence of large quantities of quartz. Minor impurities, such as illite, muscovite, halloysite, quartz hydrated mica, non-crystalline hydroxide iron and halloysite present. The presence of these minor impurities and quartz content of Ngbo clay needs to be reduced to minimum before its usage for industrial purpose especially in zeolites/catalysts development in line with researches of [28,29]. The XRD analysis corroborates with the results obtained with the XRF analysis.

Comment [A6]: Figure 1



Comment [A7]: Please attach a better quality image

Figure 1: Results of XRD analysis of Ngbo raw clay

The results of XRD pattern analysis of Ngbo acid activated clay, AAC is presented in figure 2. The results of XRD pattern results showed several characteristic peaks due to minerals compositions present. The analysis of the peaks showed sharp peaks with low intensity at $2\theta = 11.30^\circ$, which is the main peak used in the identification of kaolinite clay as reported in literature by [30].

Comment [A8]: Figure 2

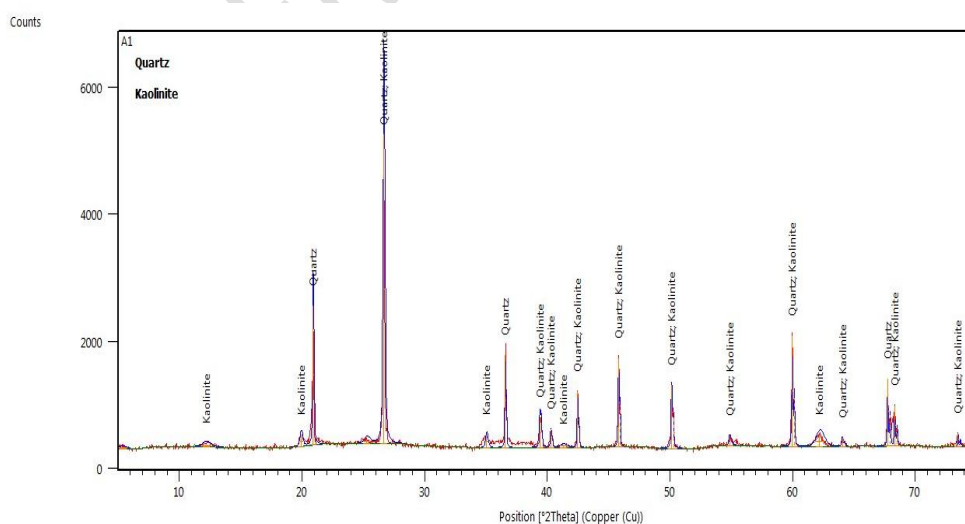


Figure 2: Results of XRD analysis of Acid Activated Clay

3.3 Esterification Process Results

Esterification technique was used to obtain the responses and yield of Acid Activated Catalyst (AAC) as shown in Table 4.

Table 4: Results showing responses and yield of AAC

| Std | Run | Factor A (°C) | Factor B (min) | Factor C (ml) | Factor D(g) | Factor E (mic) | Yield (%) |
|-----|-----|------------------|-------------------|------------------|----------------|-------------------|--------------|
| 37 | 1 | 70 | 30 | 3.75 | 0.25 | 200 | 28.89 |
| 22 | 2 | 70 | 360 | 2.5 | 0.38 | 200 | 59.78 |
| 23 | 3 | 70 | 30 | 5 | 0.38 | 200 | 8.67 |
| 29 | 4 | 70 | 195 | 2.5 | 0.38 | 100 | 59.96 |
| 26 | 5 | 90 | 195 | 3.75 | 0.25 | 200 | 37.78 |
| 1 | 6 | 50 | 30 | 3.75 | 0.38 | 200 | 48.89 |
| 32 | 7 | 70 | 195 | 5 | 0.38 | 300 | 16.94 |
| 46 | 8 | 70 | 195 | 3.75 | 0.38 | 200 | 36.00 |
| 10 | 9 | 70 | 360 | 3.75 | 0.38 | 100 | 43.47 |
| 34 | 10 | 90 | 195 | 3.75 | 0.38 | 100 | 42.18 |
| 21 | 11 | 70 | 30 | 2.5 | 0.38 | 200 | 54.22 |
| 35 | 12 | 50 | 195 | 3.75 | 0.38 | 300 | 26.68 |
| 8 | 13 | 70 | 195 | 5 | 0.5 | 200 | 14.44 |
| 4 | 14 | 90 | 360 | 3.75 | 0.38 | 200 | 46.67 |
| 2 | 15 | 90 | 30 | 3.75 | 0.38 | 200 | 30.00 |
| 11 | 16 | 70 | 30 | 3.75 | 0.38 | 300 | 26.68 |
| 31 | 17 | 70 | 195 | 2.5 | 0.38 | 300 | 56.84 |
| 3 | 18 | 50 | 360 | 3.75 | 0.38 | 200 | 34.00 |
| 24 | 19 | 70 | 360 | 5 | 0.38 | 200 | 21.78 |
| 16 | 20 | 90 | 195 | 5 | 0.38 | 200 | 22.22 |
| 44 | 21 | 70 | 195 | 3.75 | 0.38 | 200 | 37.33 |

| | | | | | | | |
|----|----|----|-----|------|------|-----|-------|
| 12 | 22 | 70 | 360 | 3.75 | 0.38 | 300 | 40.14 |
| 36 | 23 | 90 | 195 | 3.75 | 0.38 | 300 | 34.57 |
| 17 | 24 | 70 | 195 | 3.75 | 0.25 | 100 | 39.61 |
| 18 | 25 | 70 | 195 | 3.75 | 0.5 | 100 | 40.04 |
| 45 | 26 | 70 | 195 | 3.75 | 0.38 | 200 | 37.33 |
| 33 | 27 | 50 | 195 | 3.75 | 0.38 | 100 | 31.26 |
| 25 | 28 | 50 | 195 | 3.75 | 0.25 | 200 | 32.44 |
| 20 | 29 | 70 | 195 | 3.75 | 0.5 | 300 | 31.55 |
| 27 | 30 | 50 | 195 | 3.75 | 0.5 | 200 | 30.22 |
| 30 | 31 | 70 | 195 | 5 | 0.38 | 100 | 21.84 |
| 42 | 32 | 70 | 195 | 3.75 | 0.38 | 200 | 35.56 |
| 41 | 33 | 70 | 195 | 3.75 | 0.38 | 200 | 37.78 |
| 39 | 34 | 70 | 30 | 3.75 | 0.5 | 200 | 28.22 |
| 6 | 35 | 70 | 195 | 5 | 0.25 | 200 | 18.89 |
| 43 | 36 | 70 | 195 | 3.75 | 0.38 | 200 | 39.56 |
| 38 | 37 | 70 | 360 | 3.75 | 0.25 | 200 | 47.78 |
| 19 | 38 | 70 | 195 | 3.75 | 0.25 | 300 | 36.19 |
| 40 | 39 | 70 | 360 | 3.75 | 0.5 | 200 | 41.56 |
| 7 | 40 | 70 | 195 | 2.5 | 0.5 | 200 | 59.56 |
| 28 | 41 | 90 | 195 | 3.75 | 0.5 | 200 | 39.78 |
| 14 | 42 | 90 | 195 | 2.5 | 0.38 | 200 | 60.44 |
| 5 | 43 | 70 | 195 | 2.5 | 0.25 | 200 | 55.56 |
| 13 | 44 | 50 | 195 | 2.5 | 0.38 | 200 | 54.67 |
| 9 | 45 | 70 | 30 | 3.75 | 0.38 | 100 | 32.12 |
| 15 | 46 | 50 | 195 | 5 | 0.38 | 200 | 8.89 |

3.4 Analysis of Variance (ANOVA) for AAC

The ANOVA result in table 5 showed that RSM model is significant of the experimental results as indicated from the F – value of 26.60 calculated and very low probability value of $P < 0.0001$. The lack of fit F – value of 8.71 showed that it was significant and there is 1.23% chance that a Lack of Fit F – value this large could occur due to noise. The significant terms of the model was determined by F- value and P- values. The values of “Prob > F” less than 0.0500 indicate the model terms are significant while values greater than 0.100 indicate that the model terms are not significant. ANOVA involves subdividing the total variation of a set of data onto component parts. The F – value is defined as the ratio of the mean square of regression (MRR) to the error (MRe). The smaller the magnitude of the F – value, the more significant is the corresponding coefficient [31]. The regression model demonstrates that the model is highly significant as evident from the calculated F-value (207.52) and a very low probability value ($P = 0.0001$). The lack of fit F-value of 2.50 implies that it was not significant relative to the pure error and there is a 15.67% chance that a “Lack of Fit” F-value this large could occur due to noise. If P – value of lack of fit is less than 0.05, there is statistically significant lack of fit at 95% confidence level [32].

However, the result in table 6 indicates that the significant model terms A, B, C, and AB, implies that only linear effects of temperature, process duration, excess reactants, and interactive effects of temperature and process duration were significant. The model accuracy was confirmed by the correlation coefficient of the regression model which is 0.9551. The correlation coefficient showed that 95.51% of the total variation in the final concentration was attributed to the experimental variables considered in this research work. The high value of the R^2 and the “Pred R-Squared” of 0.8236 is in good agreement with the “Adj R – Squared” of 0.9192 as reported in literature by [31].

The final equation in terms of coded factors of A, B, C, and AB that indicates effects of temperature, process duration, excess reactants, and interactive effects of temperature and process duration gives:

$$\text{Yield} = + 37.26 + 2.91A + 4.84B - 20.46C - 0.74D - 2.56E + 7.89AB + 1.89AC + 1.05AD - 0.76AE + 1.89BC - 1.39BD + 0.53BE - 2.11CD - 0.45CE - 1.27DE - 0.77A^2 + 0.25B^2 + 0.40C^2 - 0.62D^2 - 0.82E^2.$$

The coefficient with one factor represent the effect of the particular factor, while the coefficients with two factors and those with second order terms represent the interaction between two factors and quadratic effect respectively (Mohd and Rasyidah 2010).

Final model equation after eliminating the insignificant terms in terms of coded variables gives: Yield = + 37.26 + 2.91A + 4.84B – 20.46C + 7.89AB (4).

Comment [A9]: No need to add (+) at the beginning of the coefficient

Table 5: ANOVA for Acid Activated Clay (AAC) catalyst

| Source | Sum of Squares | df | Mean Square | F - Value | P - Value Prob> F |
|------------------------|----------------|----|-------------|-----------|-------------------------|
| Model | 7658.64 | 20 | 382.93 | 26.60 | < 0.0001 significant |
| A - Temperature | 135.66 | 1 | 135.66 | 9.42 | 0.0051 |
| B – Process duration | 375.29 | 1 | 375.29 | 26.07 | < 0.0001 |
| C – Excess reactant | 6697.79 | 1 | 6697.79 | 465.18 | < 0.0001 |
| D – Effect of Catalyst | 8.66 | 1 | 8.66 | 0.60 | 0.4453 |
| E – Particle size | 104.50 | 1 | 104.50 | 7.26 | 0.0124 |
| AB | 249.01 | 1 | 249.01 | 17.29 | 0.0003 |
| AC | 14.29 | 1 | 14.29 | 0.99 | 0.3287 |
| AD | 4.45 | 1 | 4.45 | 0.31 | 0.5831 |
| AE | 2.30 | 1 | 2.30 | 0.16 | 0.6931 |
| BC | 14.25 | 1 | 14.25 | 0.99 | 0.3293 |
| BD | 7.70 | 1 | 7.70 | 0.53 | 0.4714 |
| BE | 1.11 | 1 | 1.11 | 0.077 | 0.7833 |
| CD | 17.85 | 1 | 17.85 | 1.24 | 0.2761 |
| CE | 0.79 | 1 | 0.79 | 0.055 | 0.8165 |

| | | | | | |
|----------------|---------|----|-------|-------|-----------------------|
| DE | 6.43 | 1 | 6.43 | 0.45 | 0.5102 |
| A ² | 5.16 | 1 | 5.16 | 0.36 | 0.5549 |
| B ² | 0.53 | 1 | 0.53 | 0.037 | 0.8495 |
| C ² | 1.39 | 1 | 1.39 | 0.096 | 0.7588 |
| D ² | 3.32 | 1 | 3.32 | 0.23 | 0.6351 |
| E ² | 5.87 | 1 | 5.87 | 0.41 | 0.5288 |
| Residual | 359.96 | 25 | 14.40 | | |
| Lack of fit | 349.91 | 20 | 17.50 | 8.71 | 0.0123 significant |
| Pure Error | 10.05 | 5 | 2.01 | | |
| Cor Total | 8018.59 | 45 | | | |

The regression model developed was also tested for by residual plots as shown in figure 3 - 5. Residual is the difference between the experimental value and value predicted by the model. This tests the assumption of constant variance of the experimental data.

Figure 3 - 5 showed the plots of predicted vs Actual response values. The plots indicate values that are not easily predicted by the model. The plot of residuals against run checks for lurking variables that may have influenced the response during the experiment. The normal plot of residuals indicates whether the residuals follow a normal distribution, and the plot of predicted against actual response values helps to detect a value, group of values that are not easily predicted by the model.

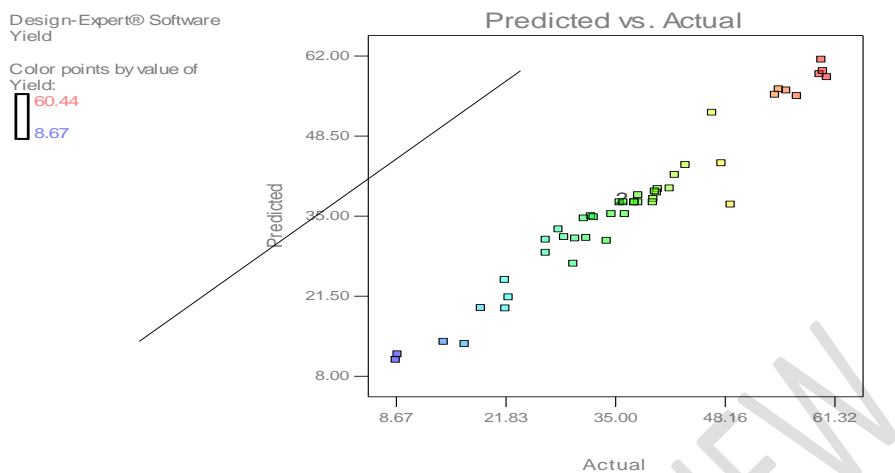


Figure 3: Residual plot of predicted vs actual for AAC

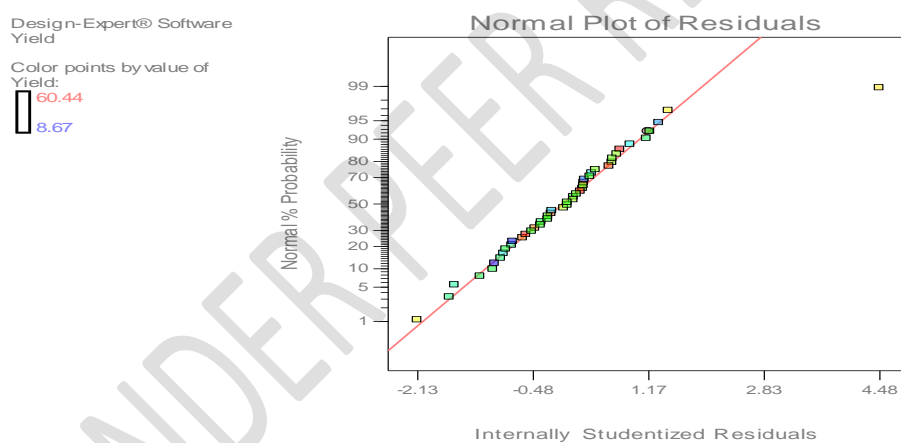


Figure 4: Normal plot of residuals for AAC

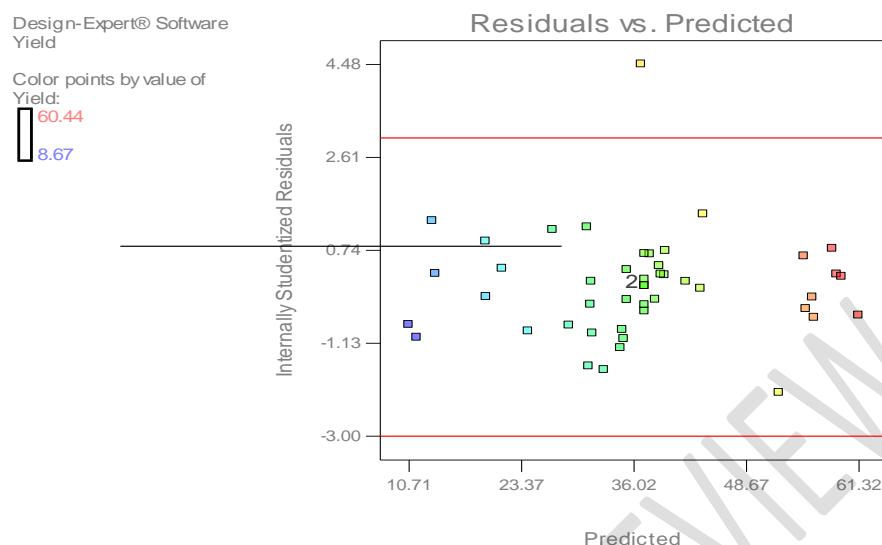


Figure 5: Residuals vs predicted for AAC

3.4.1 Contour plot of AAC

The contour plots were depicted in figure 6 to figure 14. The circular nature of the contour plots signifies that the interactive effects between the variables are not significant and the optimum values of the test process variables cannot be easily obtained [33, 31]. The non circular nature of the contour plots reveals that there is an interaction between the process variables studied and the optimum value of the process variables can be easily obtained.

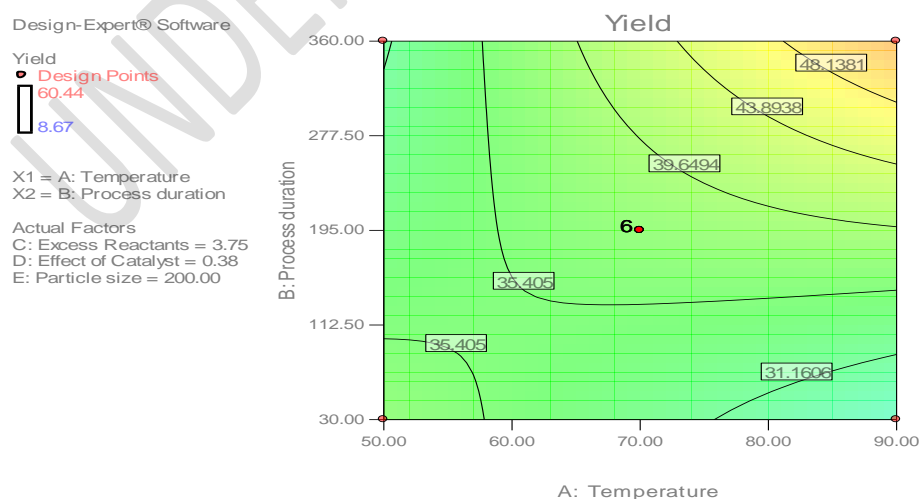


Figure 6: The contour plots for process duration against temperature and yield of AAC

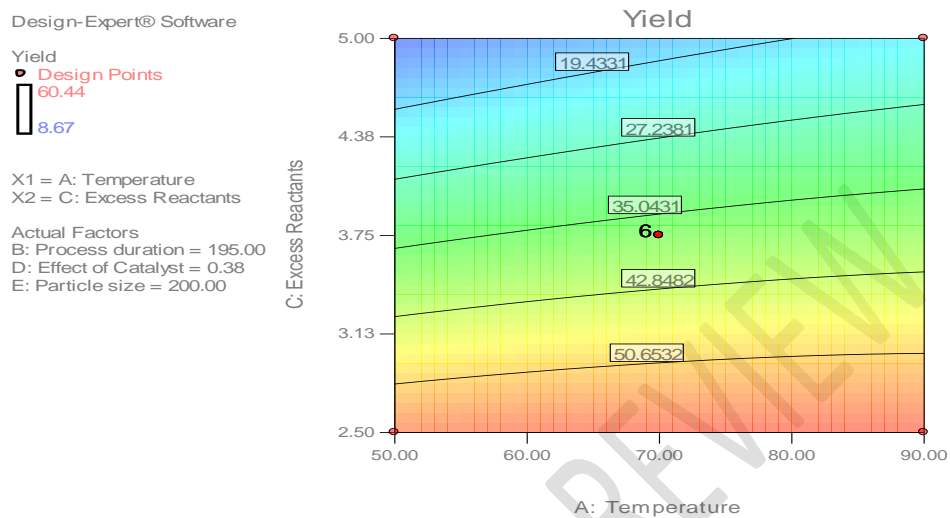


Figure 7: The contour plots for excess reactant against temperature and yield of AAC

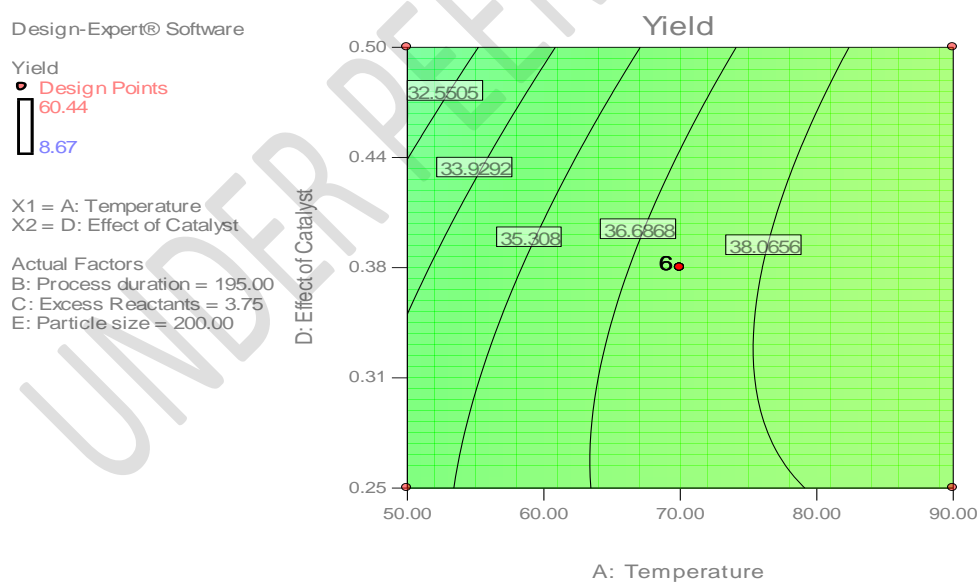


Figure 8: The contour plots for effect of catalyst against temperature and yield of AAC

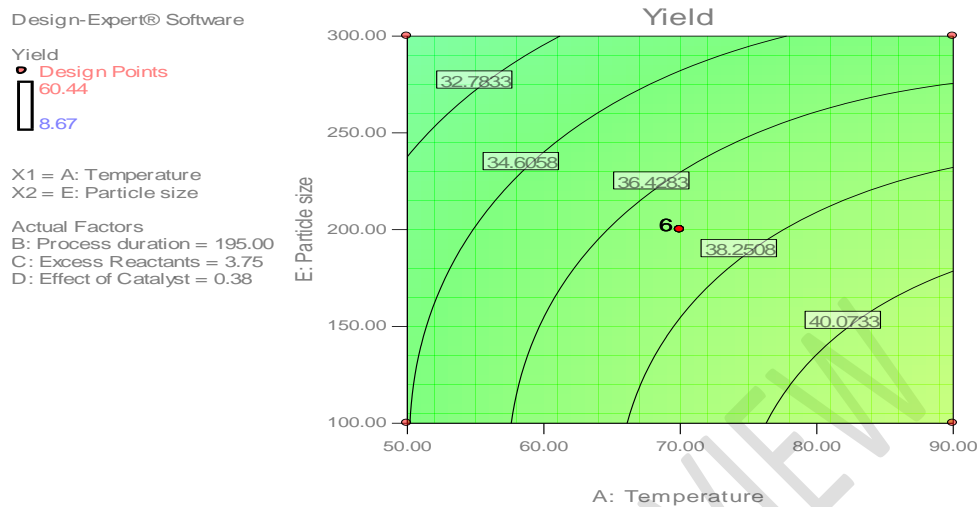


Figure 9: The contour plots for particle size against temperature and yield of AAC

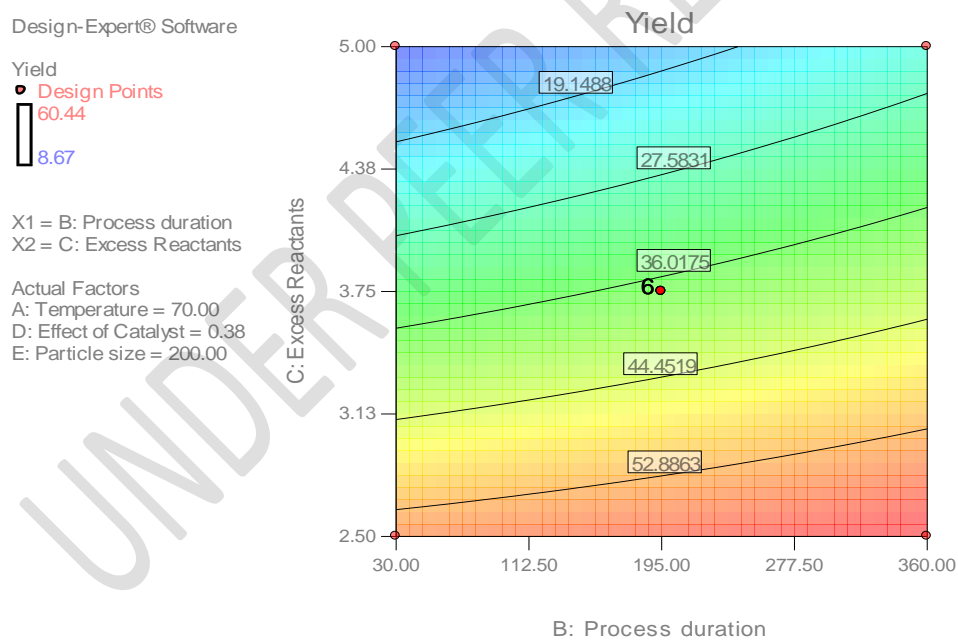


Figure 10: The contour plots for excess reactant against process duration and yield of AAC

Design-Expert® Software

Yield

● Design Points
60.44

8.67

X1 = B: Process duration

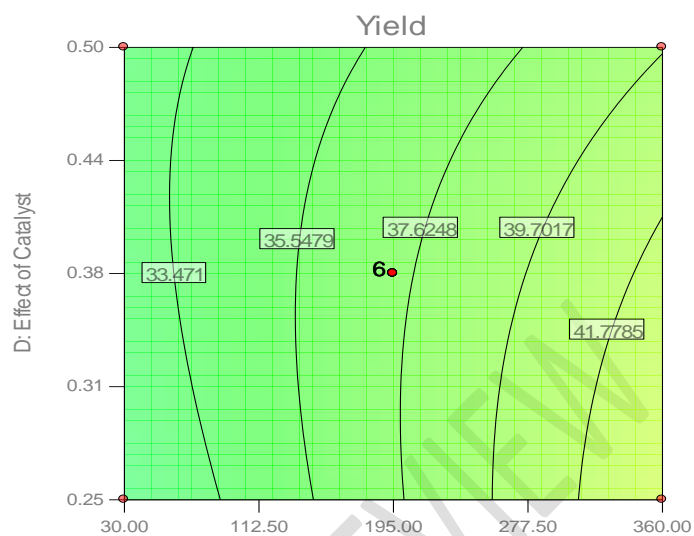
X2 = D: Effect of Catalyst

Actual Factors

A: Temperature = 70.00

C: Excess Reactants = 3.75

E: Particle size = 200.00



B: Process duration

Figure 11: The contour plots for effect of catalyst against process duration and yield of AAC

Design-Expert® Software

Yield

● Design Points
60.44

8.67

X1 = B: Process duration

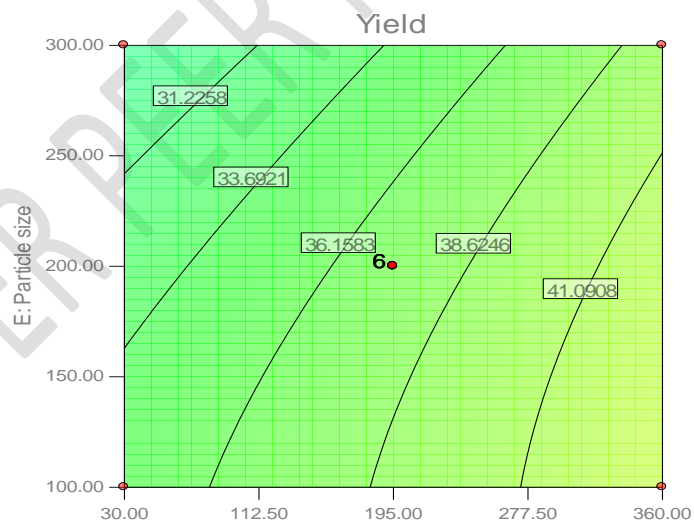
X2 = E: Particle size

Actual Factors

A: Temperature = 70.00

C: Excess Reactants = 3.75

D: Effect of Catalyst = 0.38



B: Process duration

Figure 12: The contour plots for particle size against process duration and yield of AAC

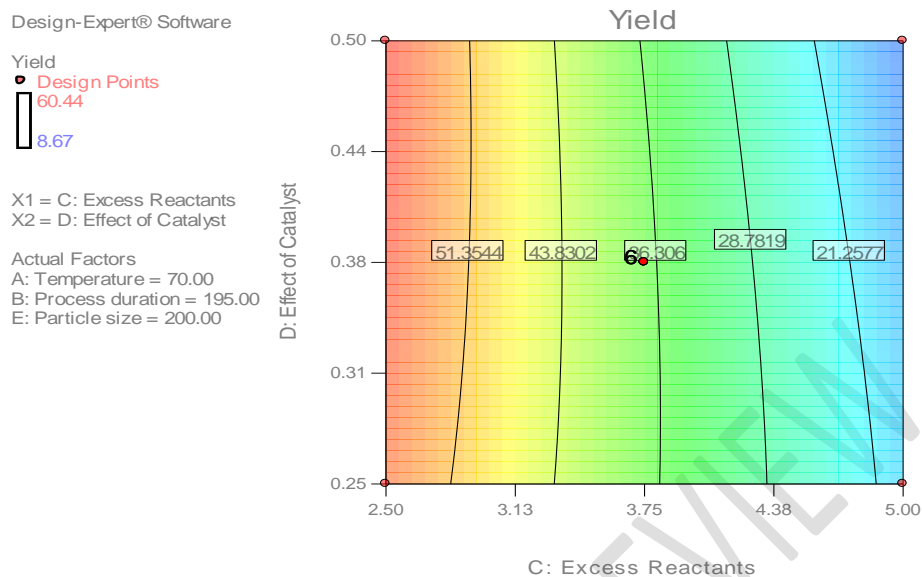


Figure 13: The contour plots for effect of catalyst against process duration and yield of AAC

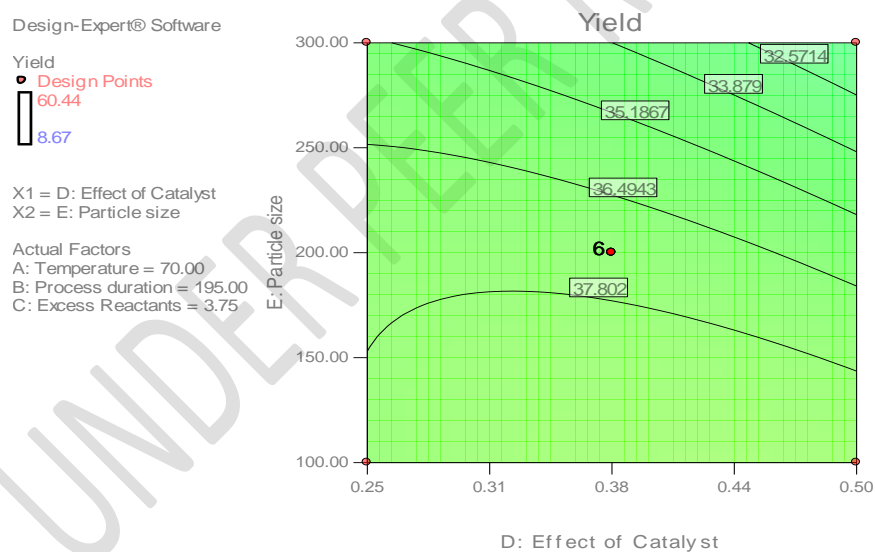


Figure 14: The contour plots for effect of catalyst against process duration and yield of AAC

3.4.2 3 – D Plot for AAC

The 3 – Dimensional plots of the response surface model are shown in figures 15 to 20. The results showed that the optimum value of the conversion was 42 for the process variables studied; which are similar to results obtained by [34, 23, 24, 35]. The three-dimensional

surfaces can provide useful information about the behavior of the system within the experiment design, facilitate an examination of the effects of the experimental factors on the responses and contour plots between the factors [33, 36,37]. The 3D plots were generated by continually varying any two variables while maintaining all other input variables constant at their null point. The 3D curves were observed to have elliptical nature with any two concerned variables. This denotes that the quadratic model chosen was appropriate with significant correlation between the two variables [38,39].

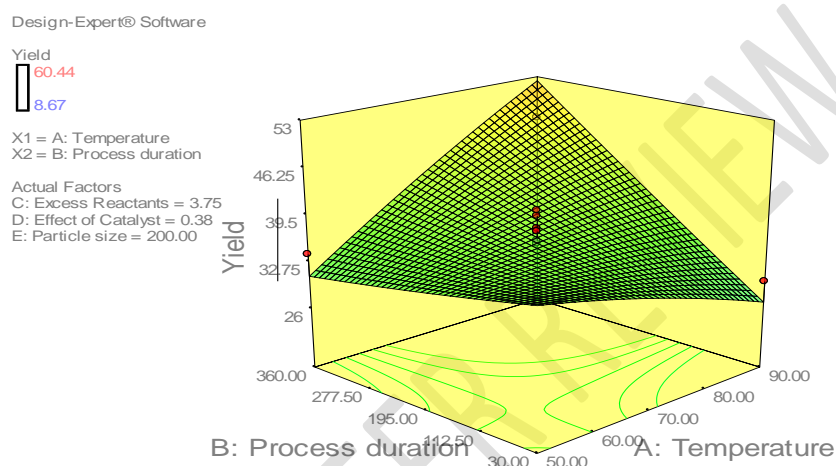


Figure 15: The 3 - D Plot for process duration against yield and temperature of AAC

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Yield
60.44
8.67

X1 = A: Temperature
X2 = D: Effect of Catalyst

Actual Factors
B: Process duration = 195.00
C: Excess Reactants = 3.75
E: Particle size = 200.00

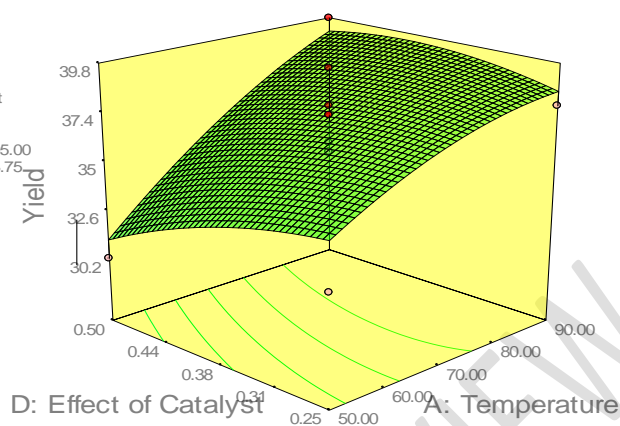


Figure 16:The 3 - D Plotfor effect of catalyst against yield and temperature of AAC

Design-Expert® Software

Yield
60.44
8.67

X1 = A: Temperature
X2 = E: Particle size

Actual Factors
B: Process duration = 195.00
C: Excess Reactants = 3.75
D: Effect of Catalyst = 0.38

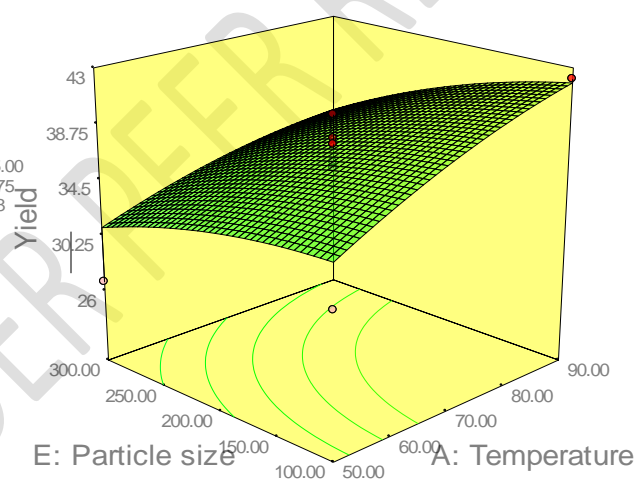


Figure 17:The 3 - D Plotfor particle size against yield and temperature of AAC

Design-Expert® Software

Yield
60.44
8.67

X1 = B: Process duration
X2 = D: Effect of Catalyst

Actual Factors

A: Temperature = 70.00

C: Excess Reactants = 3.75

E: Particle size = 200.00

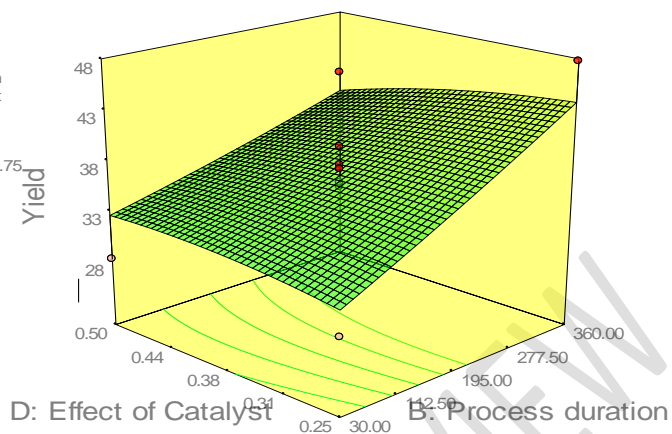


Figure 18: The 3 - D Plot for effect of catalyst against yield and process duration of AAC

Design-Expert® Software

Yield
60.44
8.67

X1 = B: Process duration
X2 = E: Particle size

Actual Factors

A: Temperature = 70.00

C: Excess Reactants = 3.75

D: Effect of Catalyst = 0.38

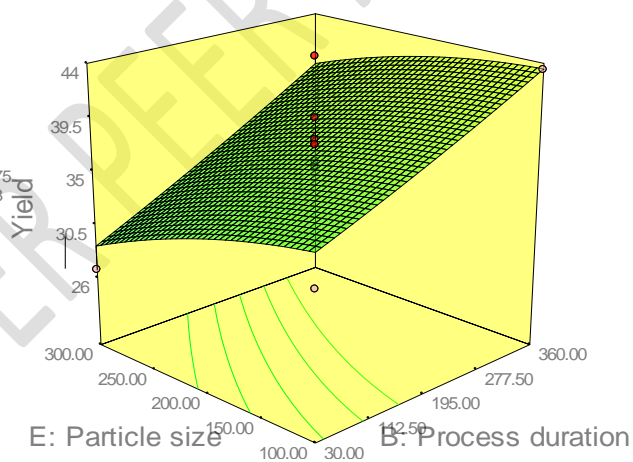


Figure 19: The 3 - D Plot for particle size against yield and process duration of AAC

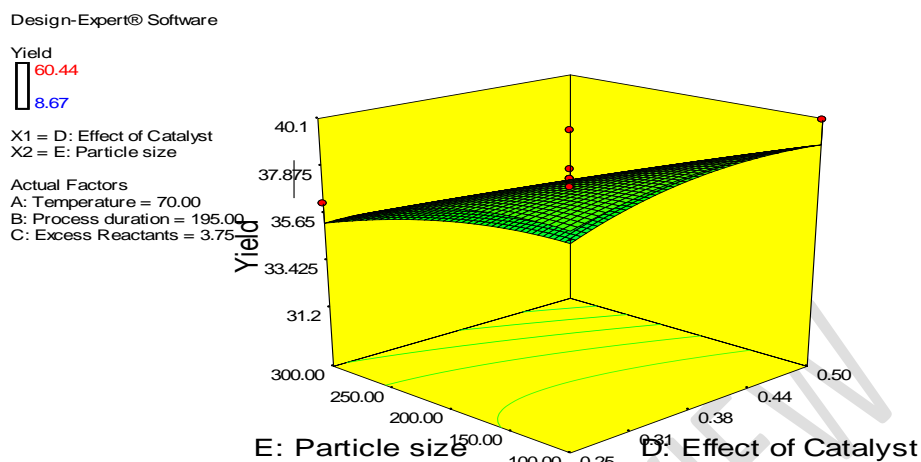


Figure 20: The 3 - D Plot for particle size against yield and effect of catalyst of AAC

3.4.3 Process Optimization

In the Process Optimization for AAC, desirability function was used to obtain the optimum value. The results of process optimisation AAC is shown in figure 21. The optimum process conditions for the variables studied were; 359.99 min, 90 °C, 4.30ml, 0.50g, and 297.63 microns for time, temperature, excess reactants, catalyst weight and particle size respectively. The predicted conversion yield was 37.5983.

Comment [A10]: It's better if there is an optimized parameter validity

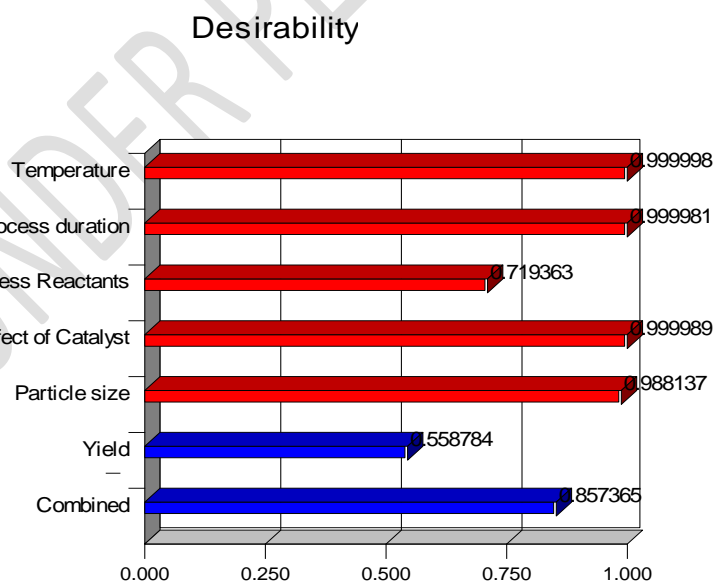


Figure 21: Process optimization for AAC

4. CONCLUSIONS

The study presented the optimum conditions for esterification reaction of acetic acid and ethanol using acid activated Ngbo clay catalyst. The optimum conditions for esterification reaction for the process conditions of temperature, duration, amount of reactant, catalyst weight and particle size was determined using Response Surface Methodology (RSM) approach. The XRF analysis showed that the clay was made of mainly SiO₂ while the XRD indicated quartz as the major composition. The predicted and experimental values from the model showed less than 5% difference thereby making the Box-Behnken design approach an efficient, effective and reliable method for the esterification of acetic acid and ethanol using acid activated clay catalyst.

Comment [A11]: Include the optimum condition in the conclusion

REFERENCES

1. Ravendra Reddy, C; Lyengar, P; Nagendrappa, G; Jai Prakash, B.S (2005).” Esterification of dicarboxylic acids to diesters over Mn⁺-montmorillonite clay catalysts” *Catalyst Letter*, 101, 87 – 91.
2. Chen C-C, Hayes KF (1999) X-ray absorption spectroscopy investigation of aqueous Co(II) and Sr(II) sorption at clay-water interfaces. *GeochimCosmochimActa* 63:3205–3215
3. Yadav, G.D;Thagathar, M.B(2002). “Esterification of maleic acid with ethanol over cation-exchange resin catalyst” *React. Funct.Polym*, 52, 99 – 110.
4. Zang, Y; Ma, L; Yang, J (2004). Kinetics of esterification of lactic acid with ethanol catalysed by cation-exchange resins” *React. Funct.Polym*, 61, 101 – 114.
5. Kirumakki S.R.; Nagaraju N; Chary, K.V.R (2006). “Esterification of alcohols with acetic acid over zeolites H β , HY and HZSM5” *Applied Catalysis A: General*, 299, 185 – 192.
6. Kirumakki S.R.; Nagaraju N; Narayanan, S.A(2004).” Comparative esterification of benzyl alcohol with acetic acid over zeolites H β , HY and HZSM5” *Applied Catalysis A: General*, 273, 1 – 9.
7. Wu, K; and Chen, Y (2004).“An efficient two-phase reaction of ethyl acetate production in modified ZSM- 5 zeolites” *Applied Catalysis A: General*, 257, 33 – 42.
8. Chu, W. Yang, X; Ye, X; Wu, Y(1996). “Vapour phase esterification catalysed by immobilized dodecatungstosilicic acid (SiW₁₂) on activated carbon”*Applied Catalysis A: General*, 145, 125 – 140.
9. Sepulveda, J.H; Yori, J.C; Vera, C.R (2005). “Repeated use of supported H₃PW₁₂O₄₀ catalysts in the liquid phase esterification of acetic acid with butanol” *Applied Catalysis A: General*, 288, 18 – 24.
10. Jermy, B.R;Pandurangan,A (2005).” Catalytic application of Al-MCM-41 in the esterification of acetic acid with various alcohol”. *Applied Catalysis A: General*, 288, 25 – 33.

Comment [A12]: check and correct the reference writing format

11. Kirumakki S.R.; Nagaraju N; Chary, K.V.R; Narayanan, S (2003). "Kinetics of esterification of aromatic carboxylic acids over zeolites H β and HZSM5 using dimethyl carbonate" *Applied Catalysis A: General*, 248, 161 – 167.
12. Nwabanne, Joseph T., Onu, Chijioke E. and Nwankwoukwu, Okwudili C. (2018) Equilibrium, Kinetics and Thermodynamics of the Bleaching of Palm Oil Using Activated Nando Clay. *Journal of Engineering Research and Reports* 1(3): 1-13. DOI: 10.9734/JERR/2018/42699
13. Ajemba R.O, Onukwuli O.D (2012) Process optimization of sulphuric acid leaching of alumina from Nteje clay using central composite rotatable design. *International Journal of Multidisciplinary Sciences and Engineering*. 2012;3(5):1–6.
14. Onu, C. E. and Nwabanne, J. T. (2014) "Application of Response Surface Methodology in Malachite green adsorption using Nteje clay". *Open Journal of Chemical Engineering and Science*. 1 (2) 19 – 33.
15. Nwobasi Veronica Nnenna, Igbokwe Philomena K., and Onu Chijioke Elijah (2020) Removal of Methylene Blue Dye from Aqueous Solution Using Modified Ngbo Clay. *Journal of Materials Science Research and Reviews*, 5(2): 33-46. May 2020
16. Onu, C. O. and Nwabanne, J. T. (2014). "Adsorption kinetics for Malachite green removal from aqueous solution using Nteje clay". *Journal of Environment and Human*. 1 (2) 133 – 150. doi: :10.15764/EH.2014.02015
17. Ezedinma Henry C., Nwabanne Josph T., E. Onu Chijioke E., and Nwajinka Charles O. (2021) Optimum Process Parameters and Thermal Properties of Moisture Content Reduction in Water Yam Drying. *Asian Journal of Chemical Sciences*, 9(4): 44-54, April 2021. DOI: <https://doi.org/10.9734/AJOCS/2021/v9i419080>
18. Onyekwelu Ijeoma U., Nwabanne Josph T., and Onu Chijioke E., (2021) Characterization and Optimization of Biodiesel Produced from Palm Oil Using Acidified Clay Heterogeneous Catalyst. *Asian Journal of Applied Chemistry Research* 8(3): 9-23, May 2021. DOI: <https://doi.org/10.9734/AJACR/2021/v8i330192>
19. Onu, C. E., Igbokwe, P. K., Nwabanne, J. T., & Ohale, P. E. (2021). ANFIS, ANN, and RSM modeling of moisture content reduction of cocoyam slices. *Journal of Food Processing and Preservation*, 00, e16032. <https://doi.org/10.1111/jfpp.16032>
20. Iheanacho Chamberlain Ositadinma, Nwabanne Joseph Tagbo and Onu Chijioke Elijah (2019) Optimum Process Parameters for Activated Carbon Production from Rice Husk for Phenol Adsorption. *Current Journal of Applied Science and Technology*, 36(6): 1-11. DOI: 10.9734/CJAST/2019/v36i630264
21. Igbokwe P. K, Nwokolo S. O, and Ogbuagu J. O, (2005).Catalytic esterification of stearic acid using a local kaolinitic clay mineral.*NJERD*, 4, 1.
22. Igbokwe P. K and Olebunne F. L,(2011). On the catalytic esterification of acetic acid with ethanol, using Nigerian montmorillonite clay: effect of reaction variables on catalyst efficiency. *Journal of the University of Chemical Technology and Metallurgy*, 46, 6, 389-394.
23. Igbokwe P. K, Ugonabo V. I, Obarandiku E, Ochili A, (2008) "Characterization and use of catalyst produced from local clay resources" *Journal of Applied Sciences (JAS)*, 2, 2.

24. Igbokwe, P.K., Olebunne, F.L., and Nwakaudu, M.S (2011)., Effect of Activation Parameters on Conversion in Clay – Catalysed Esterification of Acetic Acid, *International Journal of Basic and Applied Sciences*, 11,,5, 1 – 8,
25. Murat, M., A. Amokrane, J.P. Bastide, and L. Montanaro,(1992). “Synthesis of zeolites from thermally activated kaolinite. Some observations on nucleation and growth”.*Clay Minerals*, 27, 1, 119.
26. Akolekar, D., A. Chaffee, and R.F. Howe (1997), “The transformation of kaolin to low-silica X zeolite”. *Zeolites*, 19, 5–6, 359–365.
27. Demortier A., Golbeltz N., Letlieur J.P., Duhayon C.(1999). Infrared evidence for the formation of an Intermediate compound, during the synthesis of Zeolite Na – A from metakaolin. *International Journal of Inorganic materials*. Volume 1, issue 2, August 1999, pages 129 – 134
28. Tracy, M.M.J. and J.B. Higgins,(2001) “Collection of simulated XRD powder patterns of Zeolites” Fourth revised edition ed. 2001, Amsterdam Elsevier 379.
29. .Evamako O. Yusuf, Efeovbokhan V.E, and Babalola R. (2001). Development and characterization of zeolite – A from Elefun kaolin. *Journal of physics conference*, series 1378 – 032016.
30. Ramirez J.H, Maidonaldo – Hedar F.J, Ferez A.F, Moremo C., Costa C.A. Madeira L.M. (2007). Azo-dye orange II degradation by heterogeneous Fenton-like reaction using carbón – Fe catalysts. *Applied catalysis B: Environmental*. Volume 75, issue 3 – 4,26 September 2007, pages 312 – 323.
31. Ejikeme, M.E., P.C.N. Ejikeme, and B.N. Abalu.(2013). “RSM Optimization Process for Uptake of Water from Ethanol Water Solution Using Oxidized Starch”. *Pacific Journal of Science and Technology*. 14, 2 :319-329.
32. Azargohar, R, and A.K. Dalai(2005) “Production of Activated Carbon from Luscar Char: Experimental and Modeling Studies”. *MicroporMesopor. Mater.*85:219 – 225.
33. Anupam, K., S. Dutta, C. Bhattacharjee, and S. Datta (2011) “Adsorption Removal of Chromium (VI) from Aqueous Solution over Powdered Activated Carbon: Optimization through Response Surface Methodology. *Jornal of Hazard.Mater.*173:135 – 143.
34. Igbokwe P. K, Ugonabo V. I, Iwegbu N. A, Akachukwu P. C, Olisa C. J, (2008). Kinetics of the catalytic esterification of propanol with ethanoic acid using catalyst obtained from Nigerian clays. *Journal of the University of Chemical Technology and Metallurgy*, 345 – 348.
35. Olebunne F. L; Igbokwe P. K; Onyelucheya O. E; Osoka E. C and Ekeke I. C. (2011).“Mechanistic modeling of clay-catalysed liquid-phase esterification of acetic acid”.*Journal of Emerging Trends in Engineering and Applied Sciences*, 2, 4: 631-635.
36. Panesar, P.S. (2008).“Application of Response Surface Methodology in the Permeabilitation of Yeast Cells for Lactose Hydrolysis”.*Biochem. Eng. J.* 39:91 – 96.
37. Ahmad, A.A. and B.H. Hameed(2010) “Effect of Preparation Conditions of Activated Carbon from Bamboo Waste for Real Textile Waste Water”,*Jornal of Hazard Mater.*173:487 – 493.

38. Onu Chijioke Elijah, Igbokwe P. K., Nwabanne J. T., Nwanjinka O. C., Ohale P.E. (2020) Evaluation of optimization techniques in predicting optimum moisture content reduction in drying potato slices. *Artificial intelligence in Agriculture*. 4; 39–47. <https://doi.org/10.1016/j.aiia.2020.04.001>.
39. Onu C.E, Nwabanne J.T, Ohale P.E, Asadu C.O. (2021) Comparative analysis of RSM, ANN and ANFIS and the mechanistic modeling in eriochrome black-T dye adsorption using modified clay. *South African Journal of Chemical Engineering*; 36: 24 – 42. <https://doi.org/10.1016/j.sajce.2020.12.003>

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