Original Research Article

Evaluation Of Fade Margin in Telecommunication Network in Auchi, Nigeria

Abstract

Fading is a concept which is associated with communications, be it digital or analogue. This work deals with the

careful analysis, performance and evaluation of fade margin in a particular mobile network in Nigeria using Auchi

as a case study. With the careful analysis which were carried out on three (3) different links using some collated

data such as latitude, height of tower, power, antenna gain and model, frequency, path length and distance etc. It

was discovered that the said mobile network fade margin across the three different links was within the acceptable

range of 10db to 30db. Also, it was discovered that the longer the pathlength the higher the fade margin value as

confirmed in the results. Thus, the major characteristics needed to determine fade margin and evaluation process

were effective and realizable.

Keywords: Fade margin, Line of sight, Path length, Path profile, Sensitivity, Point to point.

1.0 Introduction

In wireless communication systems, Line of Sight (LOS) communication is a form of communication used when

the signal, such as microwave, travel in a straight line using directional antennas. When signals travel directly from the

transmitting antenna to the receiving antenna, this is referred to as line-of-sight propagation (Jabir, 2008). Microwaves are

widely used for pointtopoint communications, because their small wavelength allows conveniently-sized antennas to direct them in narrow beams, which can be pointed directly at the receiving antenna. This allows nearby microwave

equipment to use the same frequencies without interfering with each other (Gemechu, 2017).

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Fig.1.1: Mobile Communication Propagation Line of Sight (LOS)

Naturally, radio wave did not follow the natural curvature of the earth. Earth's curvature is a direct block to line-of sight communication. When enough distance separates the two radio stations so that their antennas fall behind the curvature, the earth itself blocks the transmitted signals from the receiver (Jabir, 2008). In that case, the transmitter and receiver antennas are raised and aligned to each other above the surrounding obstructions in the signal path. In order to determine the minimum antenna height for clear line of sight certain terrain and network parameters are considered; namely, the terrain elevation profile, the earth bulge, the obstruction height, the signal frequency, radius of the Fresnel zone, among others (Fidelis, 2017).

The Electromagnetic (EM) wave must propagate through non homogeneous atmosphere over a path of often mixed terrain and uneven topography. Additionally, system design constraints may require that a link be established over a path containing unavoidable man made or natural obstructions. Many of these non-free-space elements in the physical environment can cause the propagating wavefront to be absorbed, scattered, refracted, reflected, or diffracted. Reflection, diffraction, and scattering are the three basic propagation mechanisms which impact propagation in a mobile communication system. Reflection occurs when a propagating electromagnetic wave impinges upon an object which has very large dimensions when compared to the wavelength of the propagating wave. Reflections occur from the surface of the earth and from buildings and walls. For an unobstructed LOS path over relatively flat terrain, the primary source of reflections is the earth's surface. The effect of the ground reflected wavefront on the received signal is largely dependent on the distance between the transmitting and receiving antennas, the relative height of the antennas, and the reflective properties of the earth's surface.

This research work outlines the recommended methods used by Communication Infrastructure Corporation for conducting a thorough path survey, as well as key items to consider when hiring a company to install your network. Fidelis (2017) show a method for the determination of the minimum antenna mast height for line of sight wireless communication link with nonzero path inclination and with known height of one antenna that is above the maximum obstruction height of the antennas is presented. This study is aim at evaluate the performance of fade margin characteristics in communication system using three different propagation links located at Auchi, Edo State, Nigeria.

2.0 Literature review

In wireless communication systems, Line of Site (LOS) communication is a form of communication used when the signal, such as microwave, can travel in a straight line in that case, the transmitter and receiver antennas are raised and aligned to each other above the surrounding obstructions in the signal path. When signals travel directly from the transmitting antenna to the receiving antenna, this is referred to as line-of-sight propagation

In order to determine the minimum antenna height for clear line of sight certain terrain and network parameters are considered; namely, the terrain elevation profile, the earth bulge, the obstruction height, the signal frequency, radius of the Fresnel zone, among others (Rappport, 2020).

Microwave radio communications require a clear path between parabolic antennas, commonly known as a line-of-sight (LOS) condition. LOS exists when there is a direct path between two separate points and no obstructions (e.g., buildings, trees, hills, or mountains) between them. Microwave Radio waves are a type of electromagnetic radiation with wavelengths in the electromagnetic spectrum longer than infrared light. Radio waves have frequencies as high as 300 gigahertz (GHz) to as low as 30 hertz (Hz). At 300 GHz, the corresponding wavelength

A major difference in propagation through the real atmosphere versus free space is that there is air present. The two absorption peaks present in the frequency range of commercial radio links are located around 23 GHz, water molecules and 60 GHz, oxygen molecules.

2.1 Related works

Aderemi (2011) presents a study on communication link between a satellite and the Earth Station (ES) he observed a lot of impairments such as noise, rain and atmospheric attenuations. It is also prone to loss such as misalignment and polarization. It is therefore crucial to design for all possible attenuation scenarios before the satellite is deployed. Gemechu (2017), presents a thesis which aims at providing microwave radio link operating at microwave frequencies Jimma main and Agaro campuses, with the minimum objective reliability 99.999%. The designed link depends on Geo context-profiler for path profile analysis, Feko suite 5.5 for rectangular waveguide design, and link budget calculator. In the analysis there are parameters, which are significant in design of microwave link establishment: free space loss calculations, path profile analysis, fade margin, frequency planning, attenuation, rain fading predictions, reflection point's calculation, tower heights, Signal to Noise Ratio, Fresnel zone and link budget calculation. Fresnel zone clearance was considered at least at 60% of the first Fresnel zone. Volkan (2016), presents a study on optimally performing microwave communication network which begins with a properly conducted with path survey that analyzes the microwave path's characteristics to identify and mitigate all potential signal obstructions. Ultimately, a detailed path survey can reduce outage time and save money on costly repair or reinstallation bills. As the demand for point-to-point microwave transmission technology increases, the need for a properly designed and installed network becomes imperative. This paper outlines the recommended methods used by Communication Infrastructure Corporation for conducting a thorough path survey, as well as key items to consider when hiring a company to install your network. Fidelis (2017) show a method for the determination of the minimum antenna mast height for line-of-sight wireless communication link with nonzero path inclination and with known height of one antenna that is above the maximum obstruction height of the antennas is presented. This study is aimed at evaluation and performance of path profile characteristics in communication system using three different propagation links located at Auchi, Edo State, Nigeria.

3.0 Materials and Method

3.1 Materials

From the site location in Auchi, Nigeria, the data obtained were; link ID for transmitter and the receiver, latitude and longitude, Site location, Elevation (m), TX Power (dBm), Antenna gain (dBi), Antenna height (m), Frequency (MHz), Path length (km) Free space loss (dB), Atmospheric Absorption Loss (dB) and antenna model for transmitter is SC 2-W100A (TR) and the receiver is SC 2-W100A (TR) respectively. In addition, R_X sensitivity of the antenna is given as -94dBm.As shown in Fig.3.1

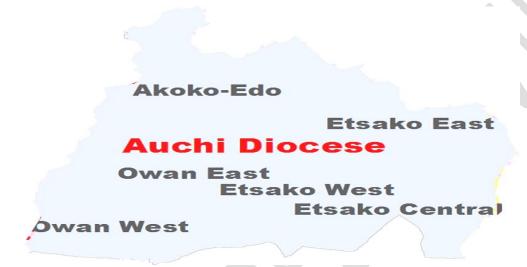


Fig.3.1: Auchi Map

That data obtained from three different locations from Network "A" are presented in Table 3.1 to Table 3.3 with the unique parameters deployed for analysis of Margin Fade characteristics.

Table 3.1: LOS Link Parameters for Point One

S/NO	LINK ID	EDO681(Transmitter)	EDO375(Receiver)		
1.	Lat.	06 1553.64 N	06 16 40.19 N		
2.	Long	005 42 30.24E	005 4102.40E		
3.	Site location	Auchi	Auchi		
4.	Circulator Branching Loss	0.50	0.50		
5.	Elevation(m)	62.03	69.08		
6.	TX Power (dBm)	24.00	24.00		
7.	Antenna model	SC 2-W100A (TR)	SC 2-W100A (TR)		
8.	Antenna gain (dBi)	34.50	34.50		
9.	Antenna height (m)	30	35		
10.	Net Path Loss (dB)	56.12	56.12		

11.	Polarization	Vertical
12.	Average Annual Temperature (⁰ C)	10°C
13.	Frequency (MHz)	11100.00
14.	Path length (km)	3.06
15.	Free space loss (dB)	123.07
16.	Atmospheric Absorption Loss (dB)	0.05

Table 3.2: LOS Link Parameters for Point Two

S/NO	LINK ID	EDO682 (Transmitter)	EDO502 (Receiver)	
1.	Lat.	06 23 06.36 N	06 23 06.14 N	
2.	Long.	005 42 21.60E	005 42 49.73E	
3.	Site location	Auchi	Auchi	
4.	Circulator Branching Loss	0.50	0.50	
5.	Elevation(m)	112.26	106.24	
6.	TX Power (dBm)	14.00	14.00	
7.	Antenna model	SB 1-220B (TR)	SB 1-220B (TR)	
8.	Antenna gain (dBm)	35.60	35.60	
9.	Antenna height (m)	25	25	
10.	Net Path Loss (dB)	49.40 49.40		
11.	Polarization	Vertical		
12.	Average Annual Temperature	10°C		
	(°C)			
13.	Frequency (MHz)	23000.00		

14.	Path length (km)	0.86
15.	Free space loss (dB)	118.43
16.	Atmospheric Absorption Loss	0.17
	(dB)	

Table 3.3: LOS Link Parameters for Point Two

S/NO	LINK ID	EDO647(Transmitter)	EDO207(Receiver)
1.	Lat.	07 05 52.08 N	07 05 22.31 N
2.	Long.	006 18 21.24E	006 17 38.80E
3.	Site location	Auchi	Auchi
4.	Circulator Branching Loss	0.50	0.50
5.	Elevation(m)	298.40	315.78
6.	TX Power (dBm)	15.00	15.00
7.	Antenna model	SB 2-190A (TR)	SB 2-190A (TR)
8.	Antenna gain (dBm)	39.00	39.00
9.	Antenna height (m)	33	35
10.	Net Path Loss (dB)	46.09	46.09
11.	Polarization	Vertical	1
12.	Average Annual	10°C	
	Temperature (⁰ C)		

13.	Frequency (MHz)	18782.00
14.	Path length (km)	1.59
15.	Free space loss (dB)	121.98
16.	Atmospheric Absorption	0.11
	Loss (dB)	

3.2 Method

3.2.1 Analysis of Margin Fade

The level of received power in excess of that required for a specified minimum level of system performance is referred to as the fade margin. So called, because it provides a margin of safety in the event of a temporary attenuation or fading of the received signal power. The minimum required received power level used for the link budget can be totally arbitrary owing to the designer's knowledge and experience but is most often tied to the receiver's sensitivity. Simply put, the receiver's sensitivity specifies the minimum RF input power required to produce a useable output signal. Typical values for receiver sensitivity fall within the range of –90 to –120 dBm.

Note: the three different locations are identified by their latitude and longitude in Auchi area, which are in the Tables.

3.2.2 Point One Analysis of Margin Fade Characteristics

Parameters from Table 3.1;

Location: Auchi

Point of Location from EDO681 to EDO375

$$FadeMargin = P_{RX} - R_X Sensitivity (3.1)$$

$$P_{RX} = P_{TX} - L_{TX} + G_{TX} - L_{Path} + G_{RX} - L_{RX}$$
 (3.2)

Where:

 P_{TX} = the transmit power in dBm.

 L_{TX} = the total system loss in dB at the transmitter.

 G_{TX} = the antenna gain in dBi at the transmitter.

 L_{PATH} = the total propagation losses in dB between the transmitter and the receiver antennas.

 G_{RX} = the antenna gain in dBi at the receiver.

 L_{RX} = the total system loss in dB at the receiver.

 P_{RX} = the receive power in dBm.

First Stage

Transmit power (P_{TX}) is given 24.00dBm

Second Stage

System loss

Surge kit loss =(-0.5), cable loss =(-1.7), connectors loss (-0.5), mismatch loss (-0.511) \approx -3.2 dB

Circulation Branching loss (dB) = 0.50 dB, atmosphere absorption loss 0.05dB

 L_{TX} = surge kit (-0.5) + cable (-1.7) + connectors (-0.5) + mismatch (-0.511) \approx -3.2 dB + Circulation Branching loss and atmosphere absorption loss (-0.55) Net Path Loss (56.12) = -59.87 dB

 L_{RX} = surge kit (-0.5) + cable (-0.85) + connectors (-0.5) + mismatch (-0.511) \approx -2.35 dB+ Circulation Branching loss and atmosphere absorption loss (-0.55) + Net Path Loss (56.12) = -59.02 dB

(3.3)

Third Stage

Antenna Gain (dBi) = 34.50

From Table 3.2

Fourth Stage

NOTE: standard atmosphere (standard refraction = k = 1.33) over a smooth earth, the distance to the RF horizon is related to the height of the antenna as follows;

$$d_{HOR} = 4.124 \sqrt{h} \tag{3.4}$$

 D_{HOR} = distance in kilometers to the RF horizon

h = the antenna height in meters above a smooth earth

$$d_{HOR} = 1.414\sqrt{h} \tag{3.5}$$

The maximum line-of-sight path distance is equal to the sum of the RF horizon distance for both the transmitting and receiving antennas:

$$LOS_{max} = 4.124 \sqrt{h_{TX}} + 4.124 \sqrt{h_{RX}}$$
 (3.6)

Where

 LOS_{max} = the maximum line-of-sight path distance in kilometers

 h_{TX} = height of the transmitting antenna in meters above a smooth earth= 30m

 h_{RX} = height of the receiving antenna in meters above a smooth earth=35m

$$LOS_{max} = 4.124 \sqrt{30} + 4.124 \sqrt{35}$$
$$LOS_{max} = 22.588 + 24.398 = 46.986km$$
$$LOS_{max} = 47.0km$$

Note: For a link to be considered as having a line-of-sight path of propagation, the distance between the transmitting and receiving antennas must be equal to or less than the maximum line-of-sight path distance:

$$d_{PATH} \le LOS_{max} = 3.06 \le 47.0$$

NOTE: 3.06 km distance path from Table (3.1) (the distance between the transmitting and receiving antennas) is less than the maximum allowable 47.0 km, this link qualifies as a LOS path of propagation.

3.3.1 Free Space Propagation Model

EM wave propagates in free space, the power density per unit area decreases in proportion to the frequency and the square of the distance traveled

These facts give rise to the classic free space loss equation:

$$FSL_{dB} = 32.45 + 20\log(d) + 20\log(f) \tag{3.7}$$

Where

FSL(dB) = free space loss in dB

d = distance in kilometers

f = frequency in megahertz

Therefore, for a distance of 3.06 km and an operating frequency of 11100.00 MHz from table 4idim:

$$FSL_{dB} = 32.45 + 20\log(3.06) + 20\log(11100.00)$$
$$FSL_{dB} = 32.45 + 9.7144 + 80.906 = 123.071$$

While free space loss alone is often used in link budget calculations, it is important to understand that in this context, the term "free space" is meant literally; no atmosphere and no reflective surfaces or obstructions of any type. This does not represent a realistic environment for earth-based telemetry links, and for many path scenarios; the use of free space loss alone will not result in a realistic link budget.

3.3.2 2-Ray Multipath Propagation Model

The EM wave must propagate through nonhomogeneous atmosphere over a path of often mixed terrain and uneven topography. Additionally, system design constraints may require that a link be established over a path containing unavoidable manmade or natural obstructions. Many of these non-free-space elements in the physical environment can cause the propagating wavefront to be absorbed, scattered, refracted, reflected, or diffracted. For an unobstructed LOS path over relatively flat terrain, the primary source of reflections is the earth's surface. The effect of the ground reflected wavefront on the received signal is largely dependent on the distance between the transmitting and receiving antennas, the relative height of the antennas, and the reflective properties of the earth's surface.

The reflected wavefront will interfere with the direct wavefront either constructively or destructively. Constructive interference occurs when the wavefronts arrive more or less in phase $(\theta_{diff} < \pm 90^{\circ})$. A 0° phase shift

with a small difference in amplitude can result in as much as 6 dB gain in received signal strength relative to the direct wavefront alone. Conversely, *destructive interference* occurs when the wavefronts arrive more or less out of phase $(\theta_{diff} > \pm 90^{\circ})$. With a phase difference of 180° and a small difference in amplitude, the wavefronts will cancel out, resulting in a null in the received signal level.

When the path distance is equal to or greater than the critical distance, the relative antenna heights become very small compared to the path distance, and the angle of incidence will approach 0°. For this path geometry, the phase shift contributable to a difference in path lengths becomes very small, and the phase shift induced in the reflected wave approaches 180° for both vertical and horizontal polarization. Under these conditions, the power density per unit area will decrease in proportion to the fourth-power of the distance, and the path loss can be calculated using the following equation:

$$PL_{2Ray} = 120 - 20\log(h_{TX}h_{rX}) + 40\log(d) \tag{3.7}$$

Where:

PL2Ray = 2-ray path loss in dB

hTX = height of the transmitting antenna in meters

hRX = height of the receiving antenna in meters

d = distance between antennas in kilometers

The critical distance (d_c) is calculated as follows:

$$d_c = \frac{4\pi h_{TX} h_{RX}}{\lambda} \tag{3.8}$$

Where

 $d_c = critical distance in meters$

 λ = wavelength of the propagating EM wave, 27.03 meters @ 11100.0 MHz

$$d_c = \frac{4 x\pi x 30 x 35}{27.03} = \frac{13,188}{27.03} = 487.9$$

$$d_c = 497.9 \text{ meter}$$

$$d_c = 0.4979 \text{ kilometer}$$

For d< d_c: calculate path loss using the free space propagation model, using Equation

For $d \ge d_c$: calculate path loss using the 2-ray propagation model, using Equation

Because the distance between antennas is 3.06 kilometers, this requires the Free Space Propagation Model (FLS).

Therefore

For $d < d_c$

$$FLS_{dB} = 32.45 + 9.7144 + 80.906 = 123.071$$

 $L_{PATH} = FLS_{dB} = 32.45 + 9.7144 + 80.906 = 123.071$
 $L_{PATH} = 123.071$

For $d \ge d_c$:

Recall Equation (3.7) the 2-Ray Multipath Propagation Model

$$PL_{2Ray} = 120 - 20 \log(h_{TX}h_{rx}) + 40 \log(d)$$

Where:

PL2Ray = 2-ray path loss in dB

hTX = height of the transmitting antenna in meters =30

hRX = height of the receiving antenna in meters =35

d = distance between antennas in kilometers = 3.06

therefore

$$PL_{2Ray} = 120 - 20 \log(30 \times 35) + 40 \log (3.06)$$

$$PL_{2Ray} = 120 - 20 \log(1050) + 40 \log (3.06)$$

$$PL_{2Ray} = 120 - 60.42 + 19.43 = 120 - 79.85 = 40.15 dB$$

Fifth Stage

3.3.3 Received Signal Level

With all the input parameters to the link budget, the power level arriving at the receiver's input can be calculated Recall Equation (3.2)

$$P_{RX} = P_{TX} - L_{TX} + G_{TX} - L_{Path} + G_{RX} - L_{RX}$$

Where:

 P_{TX} = the transmit power in dBm = 24.00dBm

 L_{TX} = the total system loss in dB at the transmitter=59.87dB

 G_{TX} = the antenna gain in dBi at the transmitter = 34.50 dBi

 L_{PATH} = the total propagation losses in dB between the transmit and receive antennas =123.071dB

 G_{RX} = the antenna gain in dBi at the receiver = 34.50 dBi

 L_{RX} = the total system loss in dB at the receiver =59.02dB

 P_{RX} = the receive power in dBm =

$$P_{RX} = 24.00 \text{dBm} - (59.87 \text{dB}) + 34.50 \text{dBi} - 123.071 dB + 34.50 \text{dBi} - (59.02 \text{dB}) = -148.96 dBm$$

Power received, using free space loss model

Sixth Stage

3.3.4 Fade Margin

Note: that the receiver's sensitivity specifies the minimum RF input power required to produce a useable output signal.

Two common methods of specifying receiver sensitivity are:

- The minimum input signal level required to limit the number of errors in the received digital data stream to a maximum Bit Error Rate (BER). A typical specification would be: –103 dBm for 1 x 10–4 BER—meaning, one bit error for every ten thousand bits received.
- The minimum input signal level required to produce a minimum SINAD ratio in the demodulated audio. SINAD is the ratio, in dB, of (Signal + Noise + Distortion) to (Noise + Distortion) and is an expression of audio quality for voice

communications. A typical specification is assumed would be: $0.28~\mu V$ for 12 dB SINAD. A somewhat subjective industry standard specifies a SINAD ratio of 12 dB as the minimum required for intelligible voice communications.

For link budget calculations, it is convenient to convert units of voltage to units of power. For a 50 Ω system (the standard for the telecommunications industry), the following equation can be used to convert volts to power in dBm: therefore

$$P_{dBm} = 10 \log \left[\frac{(Vx10^{-6})^2}{50} \right] + 30 \tag{3.9}$$

Where:

PdBm = power in dBm

V = rms voltage in microvolts

Rx Sensitivity at 0.25 uV for 12 dB SINAD

$$R_x Senitivity (P_{dBm}) = 10 \log \left[\frac{(0.25 \times 10^{-6})^2}{50} \right] + 30$$

$$R_x Senitivity (P_{dBm}) = -119 dBm$$

Therefore, fade margin for the link can be deduce using Equation (1) based on transmit power in dBm (P_{TX}) and R_X Sensitivity parameters

FadeMargin =
$$P_{RX} - R_X Sensitivity = (-148.96) - (-119dBM) = -29.96 dB$$

A link budget provides a quick, simplistic assessment of a link's viability and

The goal should be for a minimum fade margin of 20 to 30 dB. If the link budget calculations or on-site measurements indicate a fade margin of less than 10 dB, one should exercise all possible options to improve upon this figure. Some possible options are:

Use an antenna with a higher gain specification on one or both ends of the link. One should be cognizant of any FCC regulations that may put limits on the maximum radiated power for given transmitter site.

- Increase the antenna elevation at one or both ends of the link. If path obstructions or multipath interference is suspected, even a small increase (or decrease) of one-half wavelength could make a significant difference in received signal level. Any increase in system losses due to a longer transmission line are usually more than offset by the decrease in path loss.
- Add a repeater site to the path. By far, the largest factor in a link budget is path loss.

Therefore

NOTE: The receiver antenna used is SC 2-W100A (TR) with receiver sensitivity given as -94dBm from

(https://media.digikey.com/pdf/Data%20 Sheets/Linx%20 Technologies%20 PDFs/TR-xxx-SC-P.pdf)

$$R_X Sensitivity = -94dBm$$

 $FadeMargin = P_{RX} - R_X Sensitivity$

FadeMargin =
$$P_{RX} - R_X Sensitivity = (-148.96) - (-94dBM) = -54.96 dB$$

Therefore

 L_{PATH} = the total propagation losses in dB between the transmit and receive antennas =40.15dBdB

Using the 2-Ray Multipath Propagation Model

$$P_{RX} = 24.00 \text{dBm} - (59.87 \text{dB}) + 34.50 \text{dBi} - 40.15 dB + 34.50 \text{dBi} - (59.02 \text{dB}) = -65.17 dBm$$

 $Margin = P_{RX} - R_X Sensitivity = (-65.17) - (-94 dBM) = 28.83 dB$

3.4 Point two Analysis of Margin Fade Characteristics

Analysis for link 2 using Table 3.2 parameters

First Stage

Transmit power (P_{TX}) is given 14.00dBm

Second Stage

System loss

Circulation Branching loss (dB) = 0.50 dB, atmosphere absorption loss 0.17dB and Net Path Loss (49.40)

 L_{TX} = surge kit (-0.5) + cable (-1.7) + connectors (-0.5) + mismatch (-0.511) \approx -3.2 dB + Circulation Branching loss (0.50) + atmosphere absorption loss (=0.17)+ Net Path Loss (49.40) = -52.82 dB

 L_{RX} = surge kit (-0.5) + cable (-0.85) + connectors (-0.5) + mismatch (-0.511) \approx -2.35 dB+ Circulation Branching loss (0.50) + atmosphere absorption loss (=0.17)+ Net Path Loss (49.40) = **-51.97 dB**

Third Stage

From table 2

Antenna Gain (dBi) = 35.60

Fourth Stage

Path Loss

$$LOS_{max} = 4.124 \sqrt{h_{TX}} + 4.124 \sqrt{h_{RX}}$$

Where

 LOS_{max} = the maximum line-of-sight path distance in kilometers

hTX = height of the transmitting antenna in meters above a smooth earth =25

hRX = height of the receiving antenna in meters above a smooth earth= 25

$$LOS_{max} = 4.124 \sqrt{25} + 4.124 \sqrt{25}$$

 $LOS_{max} = 20.62 + 20.62 = 41.24km$
 $LOS_{max} = 41.0km$

The critical distance (d_c) is calculated as follows:

$$d_c = \frac{4\pi h_{TX} x h_{RX}}{\lambda}$$

Where

 d_c = Critical distance in meters

 h_{TX} = height of the transmitting antenna in meters=25

 h_{RX} = height of the receiving antenna in meters=25

 λ = wavelength of the propagating EM wave, 13.04 meters @ 23000.00MHz

$$d_c = \frac{4 \, x \pi x 25 \, x 25}{13.04} = \frac{7850}{13.04} = 601.99$$

$$d_c = 601.99 \, meter$$

$$d_c = 0.602 \, kilometer$$

For d< d_c: calculate path loss using the free space propagation model, using above Equation

For $d \ge d_c$: calculate path loss using the 2-ray propagation model, using above Equation(3.7)

Note d = 0.86

Therefore, the path loss will determine using the 2-ray propagation model, using Equation (3.7)

$$PL_{2Ray} = 120 - 20 \log(h_{TX}h_{RX}) + 40 \log(d)$$

Where:

PL2Ray = 2-ray path loss in dB

 h_{TX} = height of the transmitting antenna in meters =25

 h_{RX} = height of the receiving antenna in meters =25

d = distance between antennas in kilometers = 0.86

Therefore,

$$PL_{2Ray} = 120 - 20 \log(25 \times 25) + 40 \log(0.86)$$

$$PL_{2Ray} = 120 - 20 \log(625) + 40 \log(0.86)$$

$$PL_{2Ray} = 120 - 20(2.7958) + 40 \log(0.86)$$

$$PL_{2Ray} = 120 - 55.92 + (-2.62) = 61.46$$

$$PL_{2Ray} = 61.46dB$$

Received Signal Level

With all the input parameters to the link budget, the power level arriving at the receiver's input can be calculated Recall Equation (3.2)

$$P_{RX} = P_{TX} - L_{TX} + G_{TX} - L_{Path} + G_{RX} - L_{RX}$$

Where:

 P_{TX} = the transmit power in dBm = 14.00dBm

 L_{TX} = the total system loss in dB at the transmitter=52.82 dB

 G_{TX} = the antenna gain in dBi at the transmitter = 35.60

 L_{PATH} = the total propagation losses in dB between the transmit and receive antennas =61.46 dB

 G_{RX} = the antenna gain in dBi at the receiver = 35.60

 L_{RX} = the total system loss in dB at the receiver =51.97 dB

 P_{RX} = the receive power in dBm =

 $P_{RX} = 14.00dBm - (52.82dB) + 35.60dBi - 61.46dB + 35.60dBi - (51.97dB) = -81.05$ Recall equation

Fade margin =
$$P_X - R_X$$
sensitivity

Assuming

$$R_X sensitivity = -94$$

$$Fade\ margin = P_X - R_X sensitivity = (-81.05) - (-94) = 12.95$$

3.5 Point Three Analysis of Margin Fade Characteristics

Analysis for link 3 using Table 3.3 parameters

First Stage

Transmit power (P_{TX}) is given 15.00dBm

Second Stage

System loss

Circulation Branching loss (dB) = 0.50 dB, atmosphere absorption loss 0.11dB and Net Path Loss (48.09)

 L_{TX} = surge kit (-0.5) + cable (-1.7) + connectors (-0.5) + mismatch (-0.511) \approx -3.2 dB + Circulation Branching loss (0.50) + atmosphere absorption loss (=0.11) + Net Path Loss (46.09) = -49.9 dB

 L_{RX} = surge kit (-0.5) + cable (-0.85) + connectors (-0.5) + mismatch (-0.511) \approx -2.35 dB+ Circulation Branching loss (0.50) + atmosphere absorption loss (=0.11) + Net Path Loss (46.09) = -49.05 dB

Third Stage

From Table 3.3

Antenna Gain (dBi) = 39.00

Fourth Stage

Path Loss

$$LOS_{max} = 4.124 \sqrt{h_{TX}} + 4.124 \sqrt{h_{rx}}$$

Where

LOS_{max}= the maximum line-of-sight path distance in kilometers

 h_{TX} = height of the transmitting antenna in meters above a smooth earth =33

 h_{RX} height of the receiving antenna in meters above a smooth earth = 35

$$LOS_{max} = 4.124 \sqrt{33} + 4.124 \sqrt{35}$$

 $LOS_{max} = 23.69 + 24.398 = 48.09 \text{ km}$
 $LOS_{max} = 48.1 \text{ km}$

The critical distance (d_c) is calculated as follows:

$$d_c = \frac{4\pi h_{TX} x h_{rx}}{\lambda}$$

Where

d_c =Critical distance in meters

 h_{TX} = height of the transmitting antenna in meters = 33

 h_{RX} = height of the receiving antenna in meters = 35

 λ = wavelength of the propagating EM wave, 15.97 meters @ 18782.00MHz

$$d_c = \frac{4\pi h_{\text{TX}} x h_{\text{RX}}}{\lambda} = \frac{14,520}{15.97} = 909.2$$

$$d_c = 909.2 \, meter$$

$$d_c = 0.9092 \ kilometer$$

For d< d_c: calculate path loss using the free space propagation model, using Equation

For $d \ge d_c$: calculate path loss using the 2-ray propagation model, using Equation

Path length d=1.59 and $d_c=0.9092$

Therefore, the path loss will determine using the 2-ray propagation model, using Equation ()

$$PL_{2Ray} = 120 - 20\log(h_{TX} x h_{rx}) + 40\log(d)$$

Where:

 PL_{2ray} = 2-ray path loss in dB

 h_{TX} = height of the transmitting antenna in meters =33

 h_{RX} = height of the receiving antenna in meters =35

d = distance between antennas in kilometers = 1.59

Therefore,

$$PL_{2Ray} = 120 - 20 \log(33 \times 35) + 40 \log (1.59)$$

 $PL_{2Ray} = 120 - 20 \log(1155) + 40 \log (1.59)$
 $PL_{2Ray} = 120 - 20 (3.06258) + 40 \log (1.59)$
 $PL_{2Ray} = 120 - 61.25 + (8.0559) = 66.8059$
 $PL_{2Ray} = 66.81 dB$

Received Signal Level

With all the input parameters to the link budget, the power level arriving at the receiver's input can be calculated Recall above Equation

$$P_{RX} = P_{TX} - L_{TX} + G_{TX} - L_{Path} + G_{RX} - L_{RX}$$

Where:

 P_{TX} = the transmit power in dBm = 15.00dBm

 L_{TX} = the total system loss in dB at the transmitter=49.9 dB dB

 G_{TX} = the antenna gain in dBi at the transmitter = 39.00

 L_{PATH} = the total propagation losses in dB between the transmit and receive antennas = 66.81dB

 G_{RX} = the antenna gain in dBi at the receiver = 39.00

 L_{RX} = the total system loss in dB at the receiver = 49.05 dB dB

 P_{RX} = the receive power in dBm =

$$P_{RX} = 15.00 \text{dBm} - (49.9 \text{ dB}) + 39.00 \text{dBi} - 66.81 \text{dB} + 39.00 \text{dBi} - (49.05 \text{ dB}) = 72.76$$

Recall

 $Fade\ Margin = P_{RX} - R_X Sensitivity$

Assuming

R_X Sensitivity=-94dBm

Fade Margin =
$$P_{RX} - R_X$$
 Sensitivity = $(+72.76) - (-94dBm) = 21.24dB$

Locatio					iver	asmitter				el(FLS)				
Transmitter	Receiver	AntennasModel	Transmitpower (P_{TX}) dBm	Path length distance (Km)	L_{RX} total system loss (dB) receiver	$L_{{\scriptscriptstyle TX}}$ total system loss (dB) transmitter	Antenna Gain (dBi)	LOS _{MAX} (Km)	d _c Critical distance (km)	Free Space Propagation Model(FLS)	2-rayPropagation Model (dB)	P_{RX} receive power (dBm)	R _x Sensitivity(dBm)	Margin Fade (dB)
EDO6	EDO37	SC 2-	24.00	3.06	59.02	59.87	34.5	47.0	0.498	123.7	40.15	65.17	-94	28.83
81	5	W100								1				
06	06	A												
1553.6	005	(TR)												
4 N&														
005 42														
30.24E														
EDO68	ED	1-220B	14.00	0.86	51.97	52.82	35.60	41.0	0.6O 2		61.46	81.05	-119	12.95
06 23	06 23													
06.36N	06.14													
& 005	N &													
42	005													

21.60E	42												
	49.73												
	Е												
EDO64	EDO2	SB 2-	15.00	1.59	49.05	49.9	39.00	48.1	0.909	66.81	72.76	-119	21.24
		190A											
06 23	06 23	(TR)											
06.36N	06.14												
& 005	N &												
42	005												
21.60E	42												
	49.73												
	Е												

Table 3.4: key Performance Indicators parameters

The analysis of margin fades characteristics from Network "A" for the three links considered were presented in Table 3.4.

4.0 Discussion and Result Analysis

This result obtained from network 'A' from three different Mobile links location at Auchi were considered. The basic parameters associated with mobile communication fade margin were determined and presented in Table 4.1.

Table 4.1: key Performance Indicators Parameters

Number of link	Link One		Link Two		Link Three		
Link ID	EDO681	EDO375	EDO682	EDO502	EDO 647	EDO207	
	(Transmitter	(Receiver)	(Transmitter	(Receiver)	(Transmitter	(Receiver)	
)))		
Lat. and long,	06 1553.64	06 16	06 23 06.36	06 23	07 05 52.08	07 05	
	N and 005	40.19 N	N and 005	06.14 N	N and 006	22.31 N	
	42 30.24E	and 005	42 21.60E	and 005 42	18 21.24E	and 006	
		4102.40E		49.73E		17 38.80E	
Antennas Model	SC 2-	SC 2-	SB 1-220B	SB 1-	SB 2-190A	SB 2-	
	W100A(TR)	W100A(T	(TR)	220B (TR)	(TR)	190A	
		R)				(TR)	
Site location	Auchi		Auchi		Auchi		
Path length distance	3.06		0.86		1.59		
(Km)							

L_{TX} total system loss (dB) transmitter	59.87	52.82	49.9
Antenna Gain (dBi)	34.5	35.60	48.1
LOS _{MAX} (Km)	47.0	41.0	48.1
Critical distance (km)	0.498	0.602	0.909
Obtained Free Space Propagation Model (FLS) (dBm)	123.07	118.43	121.98
Calculate Free Space Propagation Model (FLS) dBm	123.71	118.37	121.95
2-ray Propagation Model (dB)	40.15	61.46	66.81
P _{RX} receiver power (dBm)	65.17	81.05	72.76
Margin Fade (dB)	28.83	12.95	21.24

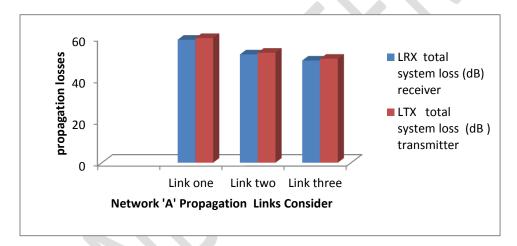


Fig. 4.1: Comparative between Transmitter and Receiver losses in dB from three different links

The comparison between total system loss in decibel at the transmitter (L_{TX}) and total system loss in decibel at the receiver show in Fig 4.1, it was observed that both transmitter and receiver total system loss in decibel are in close correlation due to hardware devices such as antenna connector, combination of coaxial cables, surge suppressors, and possibly even band pass filters used to connect the transceiver to the antenna.

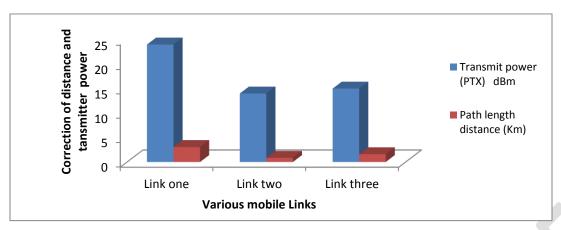


Fig. 4.2: Relationship between Transmitter Power and Path Length Distance

The transmitter power in decibel has great effects on the path length distance of microwave line of sight. Therefore, the three mobile links considered in Fig. 4.2, it was observed that increase in path length distance of microwave line of sight, will necessitate increase in transmitter power in decibel in microwave line of sight system.

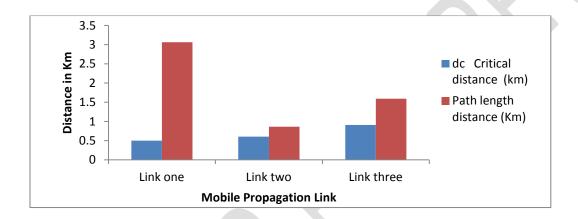


Fig. 4.3: Critical Distance and Path Length Distance

The critical distance is deduced due to environmental effect from reflection both from the ground, water body, cloud etc. The critical distance is major factor in deploying either free space propagation model or 2-Ray Multipath Propagation Model in determining the receive power in dBm.

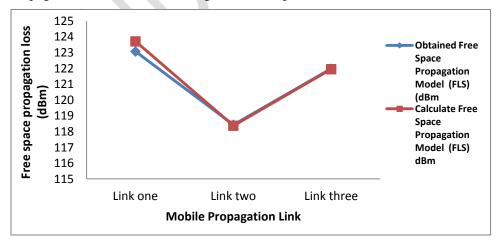


Fig. 4.4: Correlation between Obtained and Calculated Free Space Propagation Model (FLS)

The comparison between the obtained and calculated free space propagation models presented in Fig. 4.4. It was observed that both obtained Free Space Propagation Model from the field and calculated free space propagation model using Equation 3.7 possess a close correlation and attribute shown in Fig. 4.4.

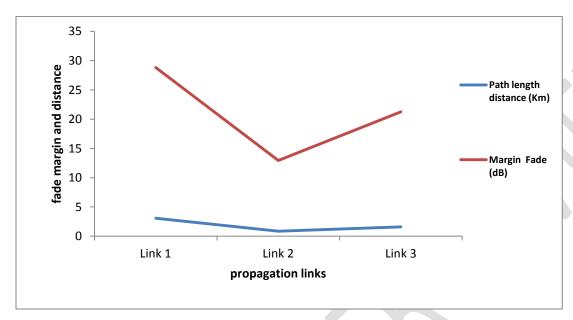


Fig. 4.5: Propagation Link for both Fade Margin and Path Length Distance

Path length distance and margin fade of the three basic mobile operator's propagation links were considered, it was observed that path length distance characteristic is affected due to the length of distance, obstacle, reflection, diffraction from ground, water bodies and atmosphere result to the pattern of radio margin fade signal obtained in receiver antenna.

The maximum receiver signal is the highest value of the received signal that is safe and would not damage the receiver. A typical value is around 20 dBm. RF telemetry link is required; the design goal should be for a minimum fade margin of 20 to 30 dB. If the link budget calculations or on-site measurements indicate a fade margin of less than 10 dB, one should exercise all possible options to improve upon this figure. Some possible options are: use an antenna with higher gain specification on one or both ends, increase the antenna elevation at one or both ends of the link, add a repeater site to the path etc.

5.0 Conclusion

Mobile communication has become a major travelling force of economic development of many countries. Therefore, the mobile communication operators are saddle with efficient service delivery, especially long-distance communication. The microwave technology using Line of Sight became paramount in mobile communication Network, which leads to the determination of fade margin of the LOS. The various fade margin characteristic parameters were determined, using existing mathematical models. Data were obtained from network "A" mobile communication network in Nigeria, three

different mobile propagation links were considered. The obtained data are link ID, Lat. & Long, Site location, Atmospheric Absorption Loss (dB), Elevation (m), TX Power (dBm), Antenna model, Antenna gain (dBi), Antenna height (m), Net Path Loss (dB), Polarization, Frequency (MHz) and Path length (km). Based on evaluation the following parameters were obtained such as margin fade (dB),receiver power (dBm), 2-ray propagation model (dB), free space propagation model (dB), LOS_{MAX} (Km)and critical distance (km) were determined. It was observed that path length distance characteristic such as the length of distance, obstacle, reflection, diffraction from ground, water bodies and atmosphere result to the pattern of radio margin fade signal obtained in receiver antenna. Thus, further work on more radio propagation links of other locations in Nigeria should be examined for proper validation.

COMPETING INTERESTS DISCLAIMER:

Authors have declared that no competing interests exist. The products used for this research are commonly and predominantly use products in our area of research and country. There is absolutely no conflict of interest between the authors and producers of the products because we do not intend to use these products as an avenue for any litigation but for the advancement of knowledge. Also, the research was not funded by the producing company rather it was funded by personal efforts of the authors.

REFERENCES

- Aderemi A. Atayero, Matthew K. Luka and Adeyemi A. Alatishe, Satellite Link Design: A Tutorial International Journal of Electrical & Computer Sciences IJECS-IJENS Vol: 11 No: 04, 2011 page 1-7
- Fidelis Osanebi Chucks Nwaduwa, Wali Samuel, Elsie Chidinma Anderson, Determination of the Minimum Antenna Mast Height with Nonzero Path Inclination: Method II, American Journal of Software Engineering and Applications, 2017; 6(2): 44-48.
- Gemechu Dengia, Tofik Jemal, and Sherwin Catolos, Microwave Link Design between Jimma Main Campus and Agaro Branch, International Journal of Engineering Research & Technology (IJERT), 2017, Vol. 6 Issue 01, page 14-21
- Jabir S. Aziz and Saba T. Hamada, Path Profile Analysis of a LOS System Using 3-D Digital Map, The 1stRegional Conference of Eng. Sci. NUCEJ Spatial ISSUE vol.11, No.1, 2008 pp 28-37
- Osahenvemwen, O.A. and Omorogiuwa, O.Rain Attenuation Analysis from System Operating at Ku and KaFrequencies Bands. American Journal of Advanced Research, ISSN: 2572-8849, Vol. 1, Number 1, pages 7-12, (http://www.ibii-us.org/Journals/AJAR/), 2017.
- Rahul Joshi, Michael D. Bond, and Craig Zilles, Targeted Path Profiling: Lower Overhead Path Profiling for Staged Dynamic Optimization Systems, Electronics, 2020, 9, 646; doi:10.3390/electronics 9040646 page 1-16.

- Segun Isaiah Popoola, and Olasunkanmi Fatai Oseni, (2014). Empirical Path Loss Models for GSM Network Deployment in Makurdi, Nigeria, International Refereed Journal of Engineering and Science (IRJES), Volume 3, Issue 6, PP.85-94.
- Surajudeen Bakinde N.T., Faruk N., Ayeni A. A., Muhammad M. Y., Gumel M.I, (2012) Comparison of Propagation Models for GSM 1800 and WCDMA Systems in Selected Urban Areas of Nigeria, International Journal of Applied Information Systems, Volume 2– No.7, Page
- Theodore S. Rappport, wireless communication principle and practice, prentice hall communication Engineering and Emerging Technologies series, Theodore S. Rappport series Edition, Page 211, 2002.
- Thilo Fath and Harald Haas, Performance Comparison of MIMO Techniques for Optical Wireless Communications in Indoor Environments, IEEE Transactions on Communications, Vol. 61, No. 2, 2013, page 733-742
- Volkan Aydın, İsmail Hakkı Çavdar, Zeynep Hasırci,Line of Sight (LoS) Probability Prediction for Satellite and HAPs Communication in Trabzon, Turkey, International Journal of Applied Mathematics, Electronics and Computers, IJAMEC, 2016, 4 (Special Issue), 155–160